

Some remarks on XS preparation with SERPENT

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Outline

- Leakage-corrected homogenized XS
- XS preparation for non-multiplying media
- Neutron multiplication due to n,xn reactions

Leakage-corrected homogenized XS

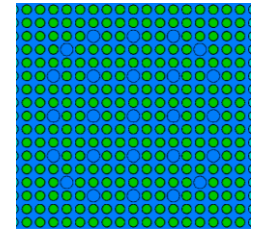
Why to introduce a leakage correction? (1)

- Heter. lattice transport calculations are performed to obtain:

- Σ_g^r, Φ_g^r in group g , for every region r with volume V^r

- Σ_g^r, Φ_g^r are homogenized into a system Σ_g^h, Φ_g^h
 - Via flux-volume and volume averaging

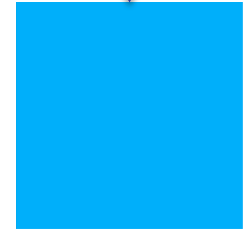
- Homogenized Σ_g^h :
 - Represent the lattice
 - To be collapsed into few-group XSs



$\Sigma_g^r, \Phi_g^r, V^r$



$$\Sigma_g^h = \frac{\sum \Sigma_g^r \Phi_g^r V^r}{\sum \Sigma_g^r V^r}$$



Σ_g^h, Φ_g^h

Why to introduce a leakage correction? (2)

- Lattice calculations are performed with reflective BC
 - Infinite lattice of identical cells
 - $k = k_{\infty}$
 - ϕ_g^h = infinite-medium flux
- The actual operating conditions are not known
 - But are normally different from the infinite lattice conditions
 - Due to the leakage effects
- What can we do?
 - To assume that the system is a part of a critical configuration
 - To force lattice $k_{\infty}=1$
 - To estimate the criticality spectrum to be used for XS collapsing
- How?
 - By introducing a leakage model

B₁ equations

- Criticality flux can be obtained by solving B₁ equations
 - Homogeneous, multi-group, dimensionless

$$\begin{cases} \Sigma_{t,g} \phi_g - \sum_{g'} \Sigma_{s,g' \rightarrow g}^0 \phi_{g'} \pm i B J_g = \chi_g \\ 3 a_g \Sigma_{t,g} J_g - 3 \sum_{g'} \Sigma_{s,g' \rightarrow g}^1 J_{g'} = \mp i B \phi_g \end{cases} \quad \text{where } a_g = f(B, \Sigma_{t,g})$$

- B₁ equations derived assuming
 - The flux separability in space, and in energy and angle
 - Linear scattering anisotropy
- The solution of B₁ equations yields:
 - Flux and net-current spectra associated with a buckling B²
 - Diffusion coefficients consistent with linearly anisotropic scattering
- The criticality flux and current spectra are found iteratively
 - By searching B² which yields k_{eff} = 1
- B1 solver is available in Serpent (version ≥ 1.14)

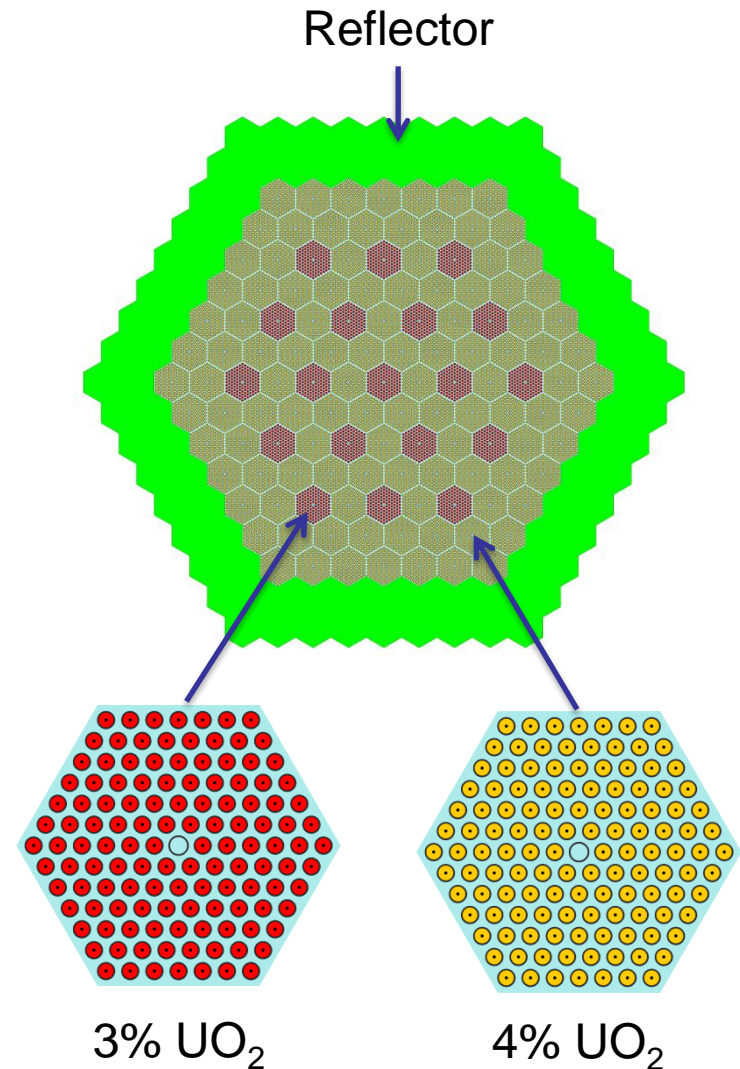
Example case: simplified VVER-440 core

Core data

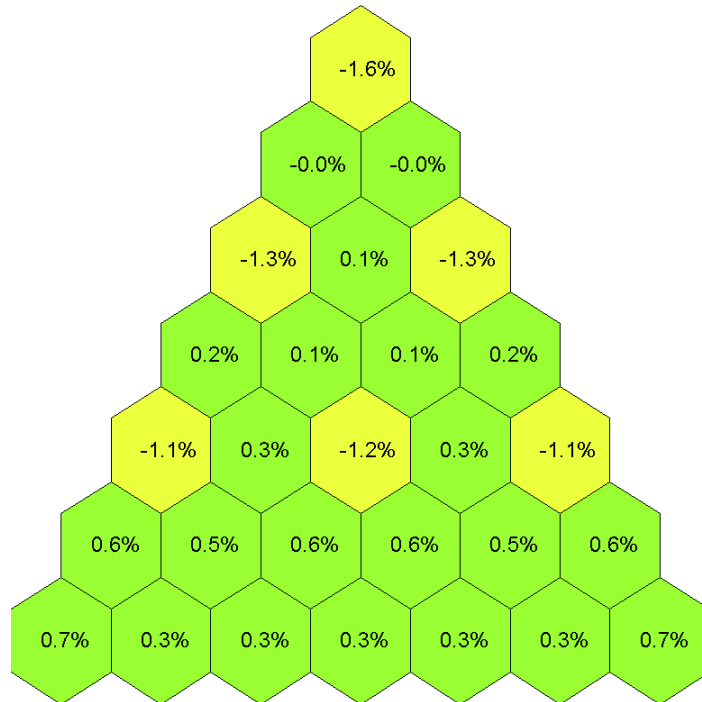
- 2D configuration
- 127 fuel assemblies
- No typical VVER-440 assembly shroud
- 90 reflector positions

In this example

- Serpent was used
 - To provide a reference solution
 - To generate two XS sets: Inf and B1
- Diffusion calculations are done by DYN3D
 - Nodal diffusion code
 - Using two XS sets
- To compare
 - K-eff
 - Radial power distribution



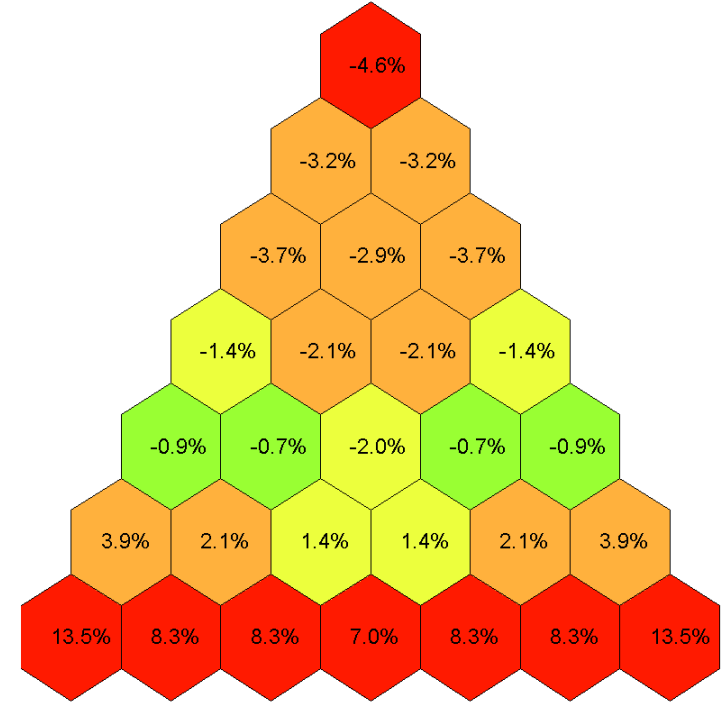
Example result: Serpent vs. DYN3D



B₁ XS

Difference in radial power:
Max.=**1.6%** RMS=**0.5%**

Difference in k_{eff} :
 $\Delta k/k =$ **-0.20%**



Inf XS

Difference in radial power:
Max.=**13.5%** RMS=**6.1%**

Difference in k_{eff} :
 $\Delta k/k =$ **0.74%**

P1 vs. B1 diffusion coefficients

	g1	g2
P1	1.208	0.364
B1	1.473	0.457
Rel. diff	-21.9%	-25.6%

Reflector modeling

Generation of reflector XS for nodal codes

Some background

- To get a “good” nodal solution one should preserve:
 - Node-averaged reactions rates (RR)
 - Surface-averaged net leakage rates (LR)
- This is done via the use of:
 - Flux-volume weighted (FVW) XS
 - Discontinuity factors (DF):

$$DF = \frac{\phi_s^{het}}{\phi_s^{hom}}$$

ϕ_s^{het} – surface flux from heter. transport solution

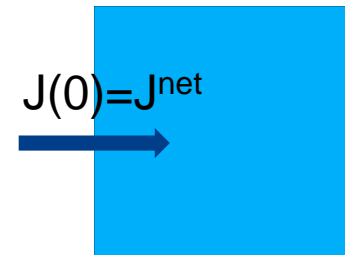
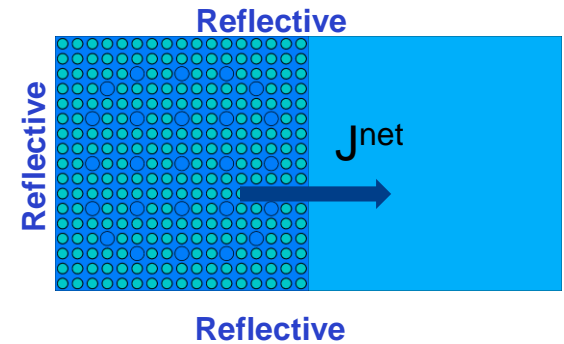
ϕ_s^{hom} – surface flux from homog. diffusion solution obtained with FVW XS

- For a single reflected fuel assembly:
 - ϕ_s^{hom} can be replaced by averaged ϕ^{het} (K. Smith)
 - This is the way how DF are calculated in Serpent
 - **Not valid for reflector regions**

Generation of reflector XS for nodal codes

How it's done with deterministic transport lattice codes

- Solve 1D heter. fuel-reflector (F/R) problem
 - To obtain homogenized XS,
F/R interface fluxes and currents
- Solve 1D homo. diffusion equation with a fixed source
 - Separately for the fuel and reflector regions
 - Using homogenized XS
 - Using net currents as a boundary condition
 - To obtain diffusion surface flux
- Calculate DF
 - as a ratio between transport and diffusion surface fluxes



Generation of reflector XS for nodal codes

Estimation of the leakage rates in Serpent

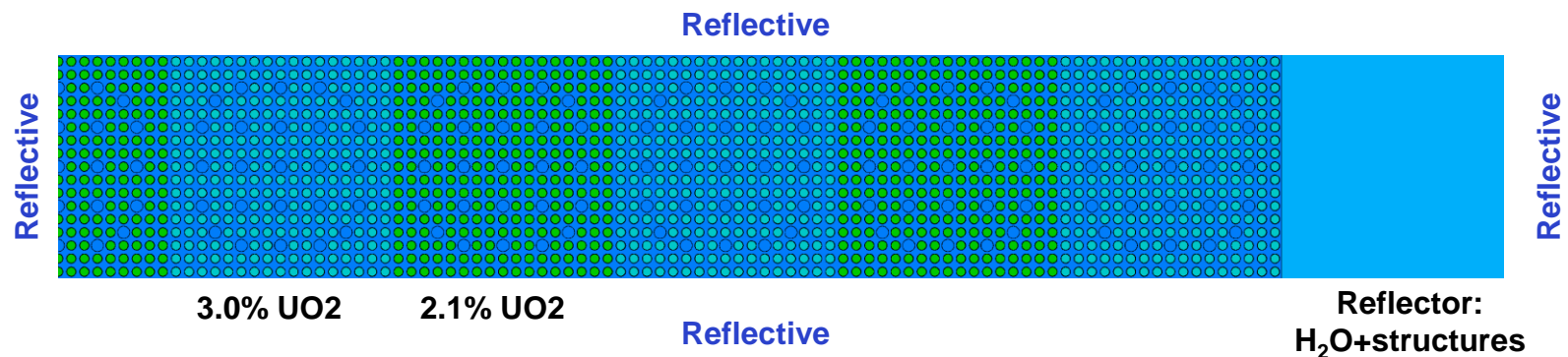
- Homogenized XS are directly available
- Interface currents are not
 - In Serpent there is no MCNP F1-like surface current tally
- How to estimate the leakage?
 - Via the use of MCNP – not “sustainable” solution
 - Via the nodal neutron balance
 - “Elegant” solution - requires minor additional effort
 - Proposed by Bryan Herman of MIT

$$LR_g + \Sigma_{t,g} \phi_g = \sum_{h=1}^G v \Sigma_s^{h \rightarrow g} \phi_h + \frac{\chi_g}{k} \sum_{h=1}^G v \Sigma_{f,h} \phi_h$$

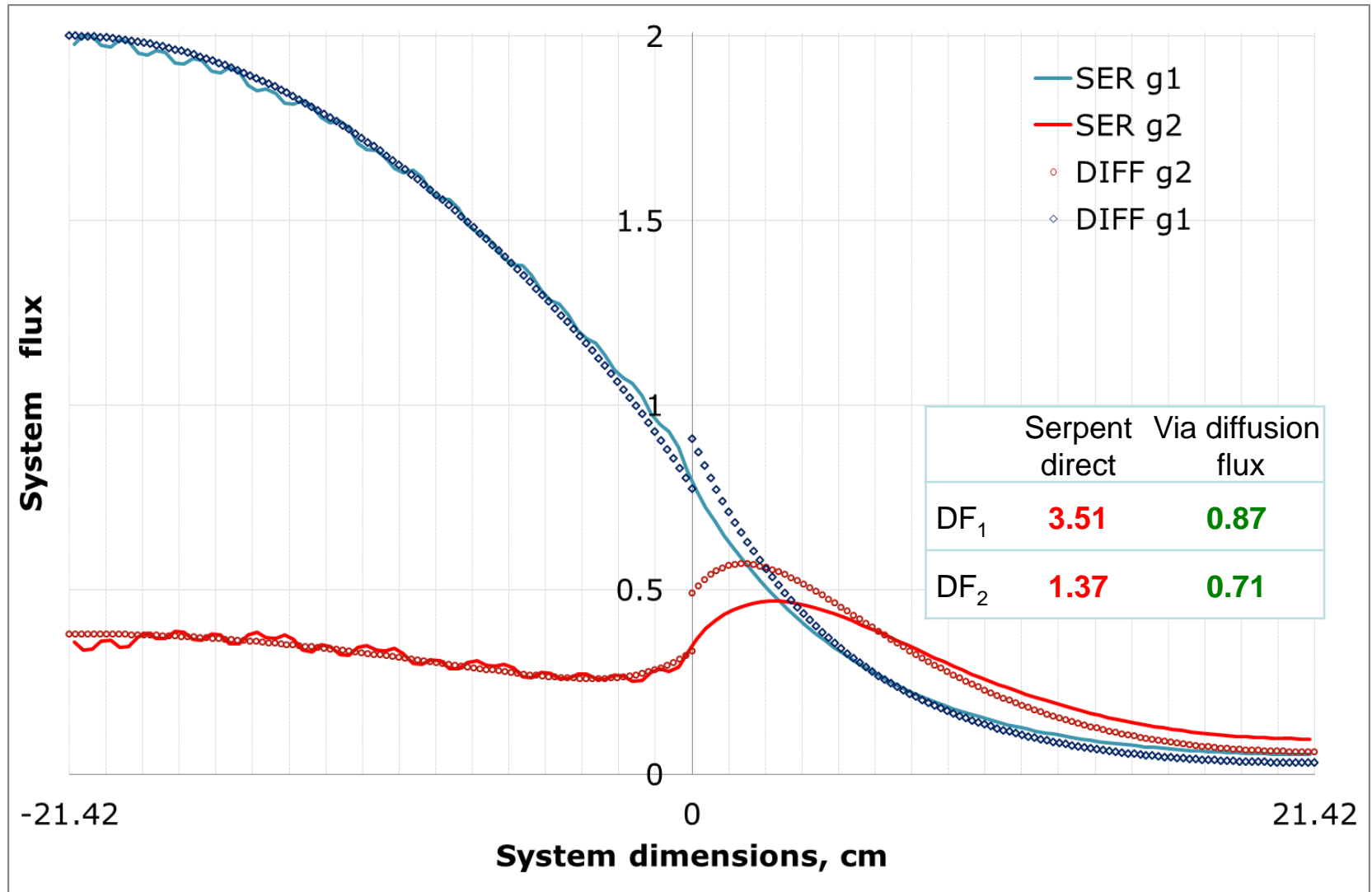
Generation of reflector XS for nodal codes

A test problem

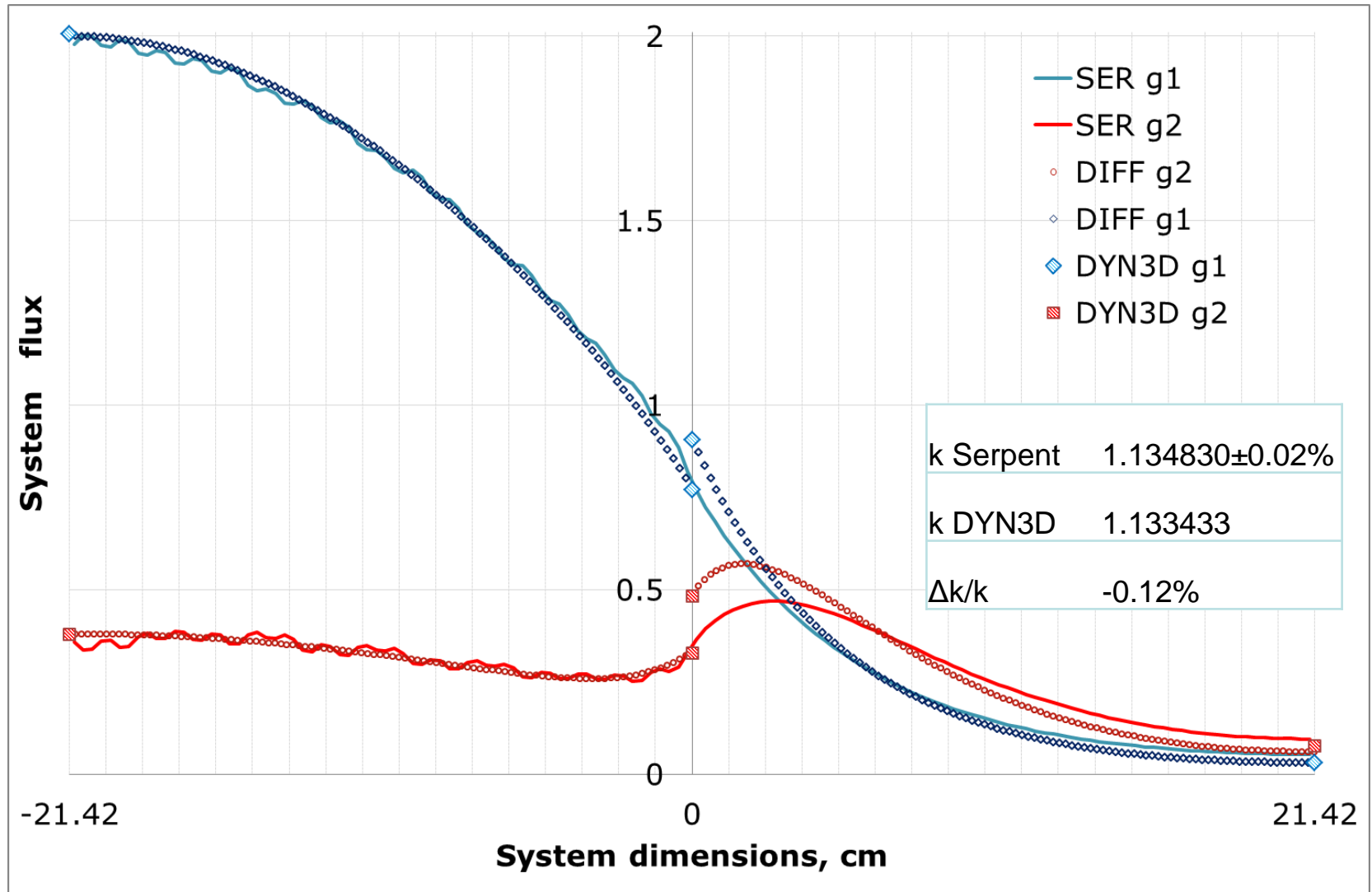
- A single row of PWR fuel assemblies with reflector
- Serpent was used
 - To generate 2-G homogenized XS for the nodal diffusion code DYN3D
 - To provide a reference solution
- The compared parameters:
 - K-eff
 - Nodal power distribution



Flux in the F/R region



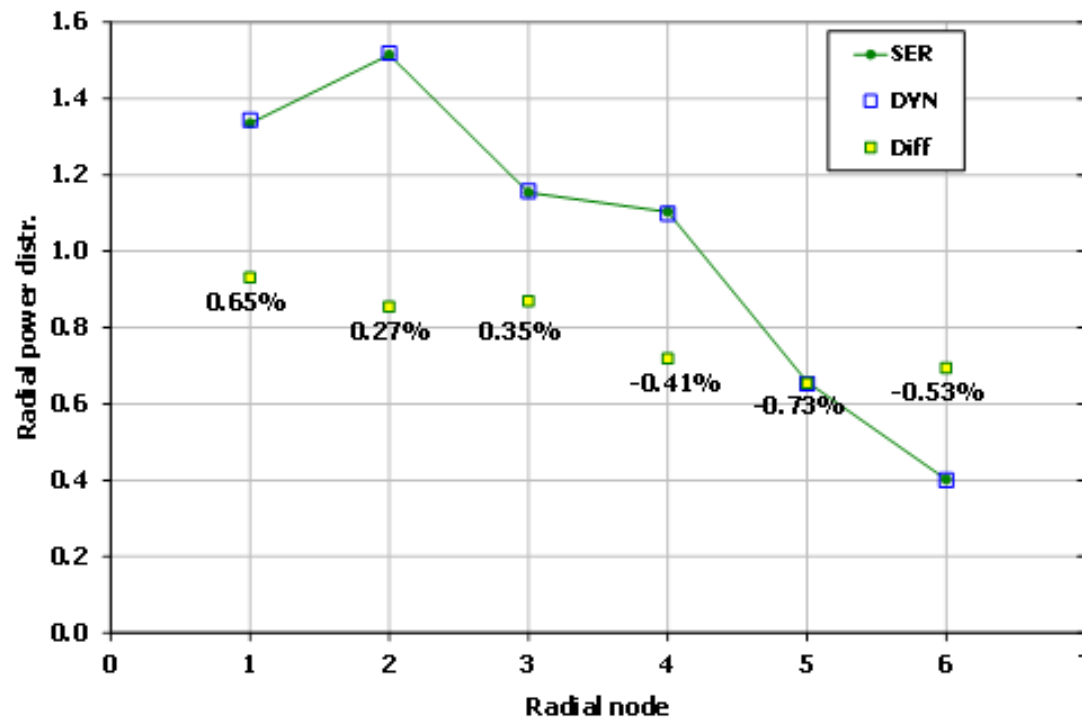
Flux in the F/R region



Generation of reflector XS for nodal codes

Results of the test case

	k-eff	$\Delta k/k$
SERPENT	1.28148	
DYN3D	1.27990	0.12%
$\sigma_{k\text{-eff}}=0.005\%$		



Neutron multiplication due to n,xn reactions

Neutron multiplication due to n,xn reactions

Neutron balance for group g , leakage excluded:

$$\overbrace{\Sigma_{a,g}\phi_g + \Sigma_{n1n,g}\phi_g + \Sigma_{n2n,g}\phi_g + \Sigma_{n3n,g}\phi_g \dots}^{\Sigma_{t,g}}$$

$$= \overbrace{\sum_{h=1}^G \Sigma_{n1n}^{h \rightarrow g} \phi_h + 2 \sum_{h=1}^G \Sigma_{n2n}^{h \rightarrow g} \phi_h + 3 \sum_{h=1}^G \Sigma_{n3n}^{h \rightarrow g} \phi_h \dots}^{\text{Full in-group scattering source}} + \overbrace{\frac{1}{k} \chi_g \sum_{h=1}^G \nu \Sigma_{f,h} \phi_h}^{\text{Fission source}}$$

In previous Serpent versions (before ver. 1.15):

- Only GTRANSFXS (group transfer XS matrix) was available
- $\text{GTRANSFXS} = \Sigma_{n1n}^{h \rightarrow g}$

Neutron multiplication due to n,xn reactions

The direct use of GTRANSFXS effectively means:

$$\overbrace{\Sigma_{a,g}\phi_g + \Sigma_{n1n,g}\phi_g + \Sigma_{n2n,g}\phi_g + \Sigma_{n3n,g}\phi_g \dots}^{\Sigma_{t,g}} =$$

$$= \underbrace{\sum_{h=1}^G \Sigma_{n,1n}^{h \rightarrow g} \phi_h + 2 \sum_{h=1}^G \Sigma_{n,2n}^{h \rightarrow g} \phi_h + 3 \sum_{h=1}^G \Sigma_{n,3n}^{h \rightarrow g} \phi_h \dots}_{\text{Full in-group scattering source}} + \underbrace{\frac{1}{k} \chi_g \sum_{h=1}^G \nu \Sigma_{f,h} \phi_h}_{\text{Fission source}}$$

The question: how to account for n,xn reactions ($x > 1$) correctly?

Neutron multiplication due to n,xn reactions

Typical few-group XS libraries used by nodal codes:

- Can contain **only** a single group transfer XS matrix
- Some re-arrangement of neutron balance equation is required

1. Lump all n,xn XS into the one **production** scattering XS:

$$\nu\Sigma_s = \Sigma_{n1n} + 2\Sigma_{n2n} + 3\Sigma_{n3n} + \dots$$

2. Re-write Σ_t in terms of $\nu\Sigma_s$ and $\Sigma_{n,xn}$

$$\Sigma_t = \Sigma_a + \nu\Sigma_s - (\Sigma_{n2n} + 2\Sigma_{n3n} + \dots)$$

3. Define a modified Σ_a

$$\Sigma_a^{\text{mod}} = \Sigma_a - (\Sigma_{n2n} + 2\Sigma_{n3n} + \dots)$$

4. Re-write the balance equation in terms of $\nu\Sigma_s$ and modified Σ_a

$$\Sigma_{a,g}^{\text{mod}} \phi_g + \nu\Sigma_{s,g} \phi_g = \sum_{h=1}^G \nu\Sigma_s^{h \rightarrow g} \phi_h + \frac{1}{k} \chi_g \sum_{h=1}^G \nu\Sigma_{f,h} \phi_h$$

Neutron multiplication due to n,xn reactions

Relevant modifications in few-group XS in Serpent 1.15

- Modifications
 - GTRANSFXS now includes **all** n,xn reactions
- New XS types
 - SCATTPRODXS = **production** scattering XS ($\nu\Sigma_s$)
 - GPRODXS = **production** group transfer XS matrix ($\nu\Sigma_s^{h\rightarrow g}$)
 - RABSXS = **modified** absorption XS (Σ_a^{mod})

Neutron multiplication due to n,xn reactions

Numerical example

Test case: typical PWR fuel assembly

	k-inf	Diff, pcm
SERPENT MC	1.33419 ± 7pcm	-
Neutron balance in 2g using ABSXS + GTRANSFXS	1.33204	-121
Neutron balance in 2g using RABSXS + GPRODXS	1.33407	-8

In deterministic codes...

From Helios methods:

II. 5.3 Cross-section adjustments for $(n,2n)$ and $(n,3n)$

II. 5.3.1 Reactivity effects

To avoid the use of $(n,2n)$ and $(n,3n)$ cross-sections in the transport calculations, their effect is included in the definitions of the absorption cross-sections and scattering matrices in the library. This is done as follows:

$$\left. \begin{aligned} \sigma_a &\rightarrow \sigma_a' = \sigma_a - \sigma_{n2n} - 2\sigma_{n3n} \\ \sigma_s &\rightarrow \sigma_s' = \sigma_s + 2\sigma_{n2n} + 3\sigma_{n3n} \end{aligned} \right\}. \quad (40)$$

Summary

- In this presentation you saw
 - Some issues associated with few-group XS generation
 - As well as possible solutions
 - Supported by numerical examples
- Serpent can be used for few-group XS generation
 - For both multiplying and non-multiplying media
- Future work
 - Automatic scripts for branching calculations and data management
 - Generation of the data for transient nodal calculations
 - Verification via existing numerical benchmarks
 - RIA, boron dilution, etc

Thank you!