



## Modeling core deformations and related reactivity effects in SFRs

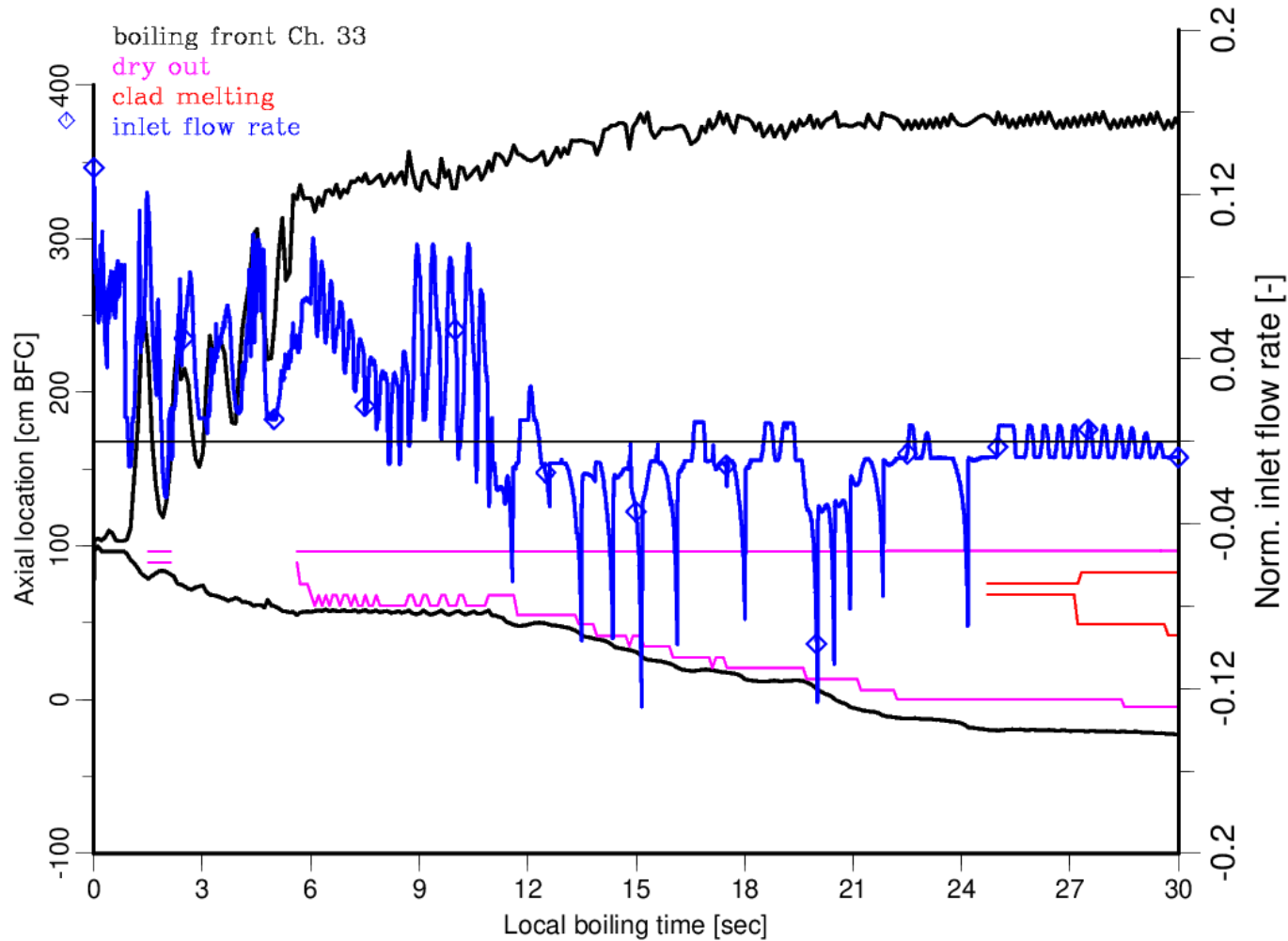
Speaker:	Emil Fridman
Affiliation:	HZDR, Dresden
Event:	Serpent UGM
When:	August, 2022
Where:	TUM, Garching



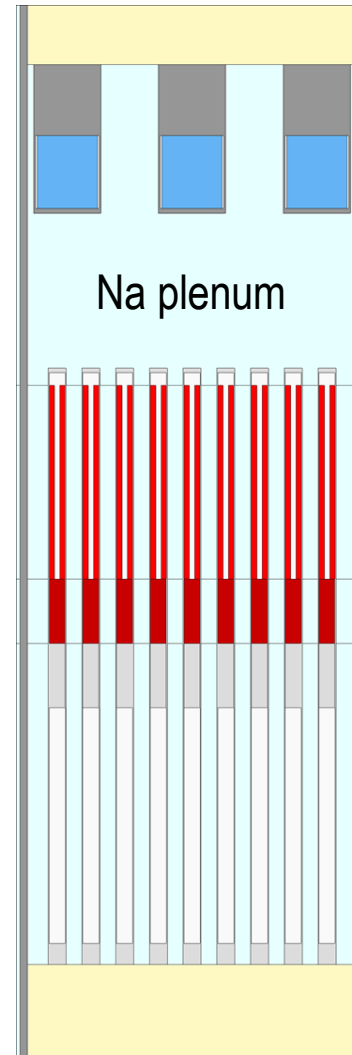
- Motivation and goals
- Methods to model reactivity effects cause by core deformations
- Application to the Phenix core



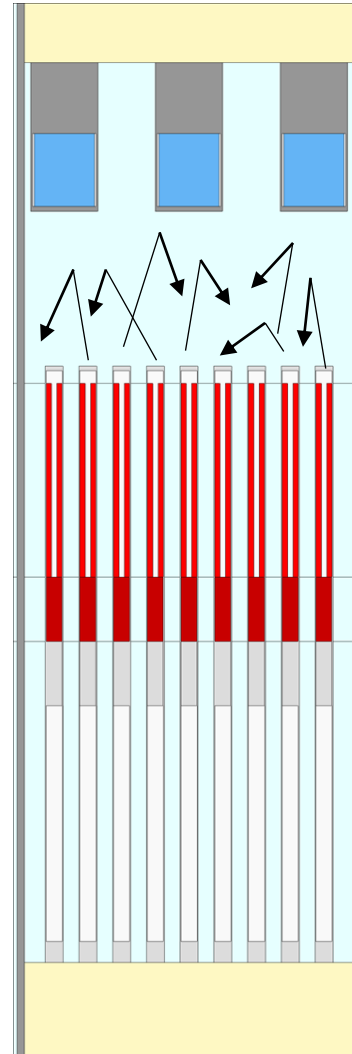
# ULOF in SFR: boiling, dry-out and clad melting fronts



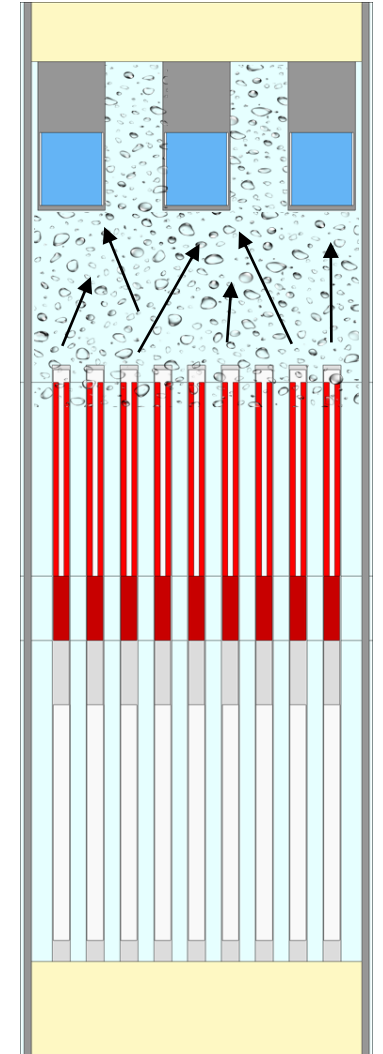
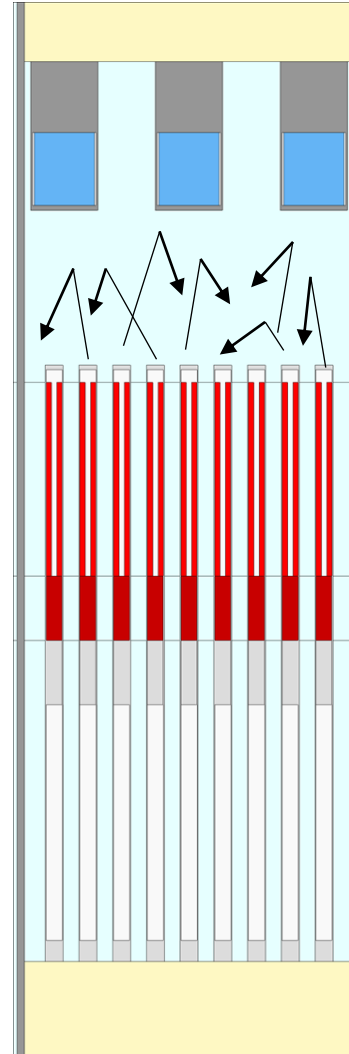
- ESFR fuel SA design
  - No upper fertile blanket
  - Large sodium plenum
  - Upper neutron absorber



- ESFR fuel SA design
  - No upper fertile blanket
  - Large sodium plenum
  - Upper neutron absorber

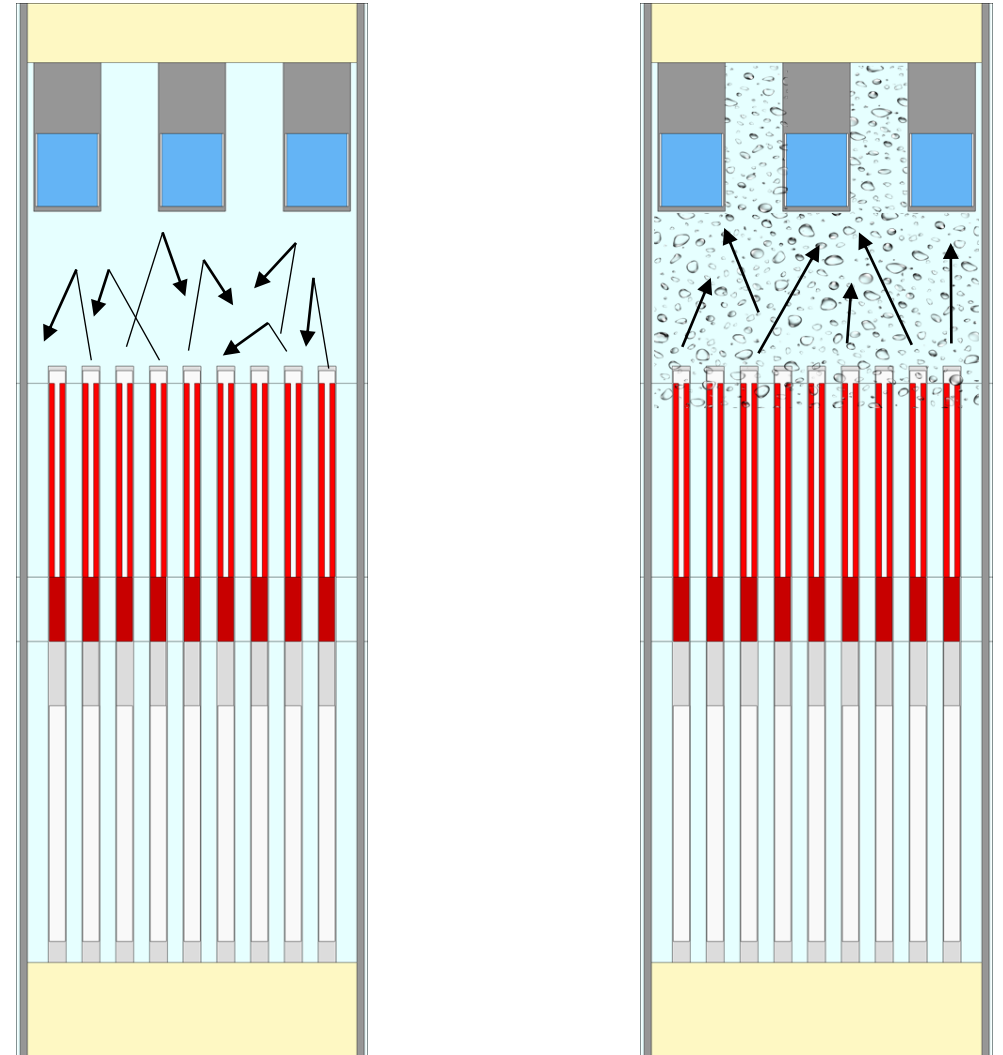


- ESFR fuel SA design
  - No upper fertile blanket
  - Large sodium plenum
  - Upper neutron absorber
- In case of sodium boiling (e.g. ULOF)
  - Reduced reflection towards active core
  - Increased leakage towards neutron absorber

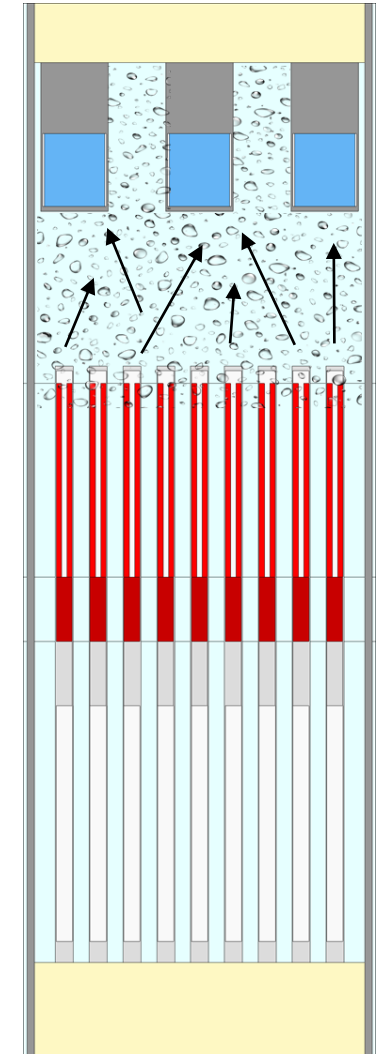
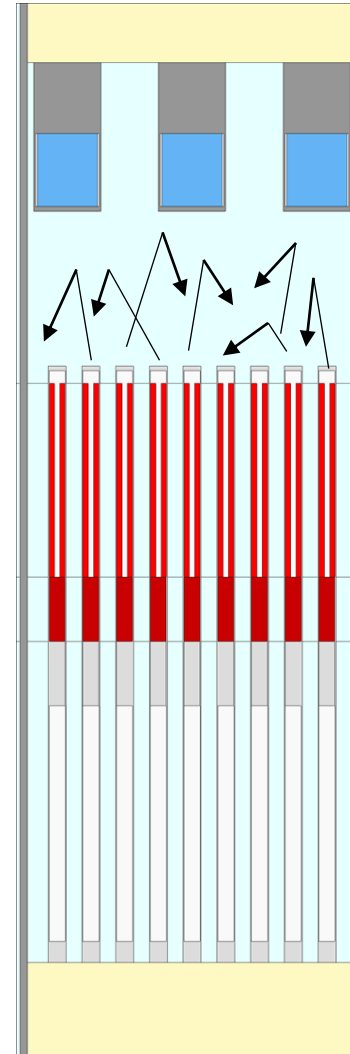


- ESFR fuel SA design
  - No upper fertile blanket
  - Large sodium plenum
  - Upper neutron absorber
- In case of sodium boiling (e.g. ULOF)
  - Reduced reflection towards active core
  - Increased leakage towards neutron absorber

→ low Sodium Void Reactivity Effect (SVRE)



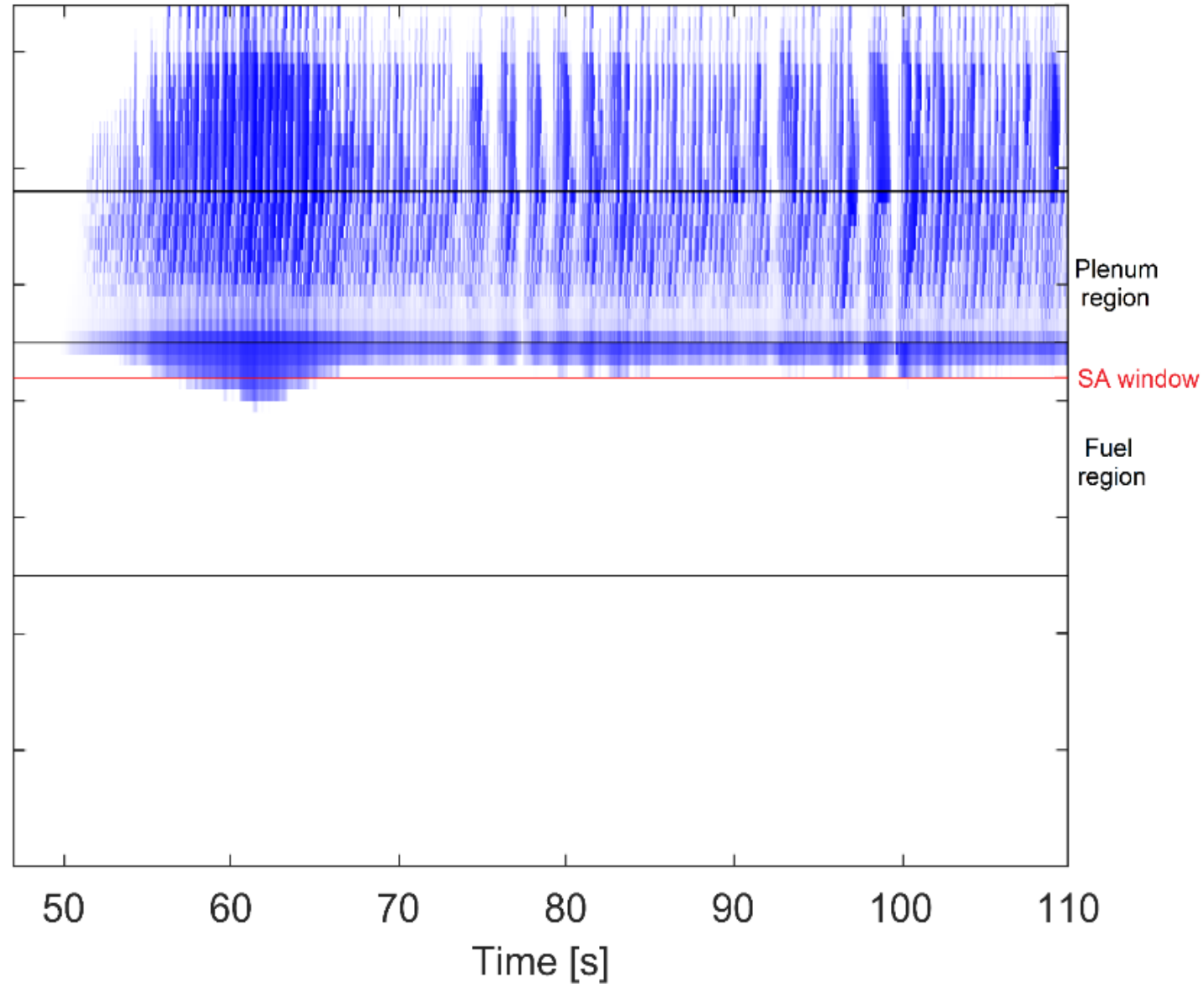
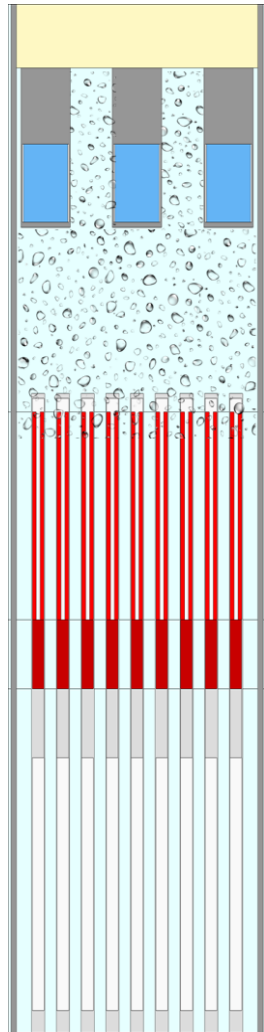
- Potential to stabilize reactor during ULOF
  - No reactivity excursion
  - No power runaway
  - Stabilized sodium boiling
  - No permanent dryout
- Potential for the chugging boiling regime
  - Periodic generation / collapsing of the sodium vapor bubbles







# Void fraction in fuel SA during ULOF





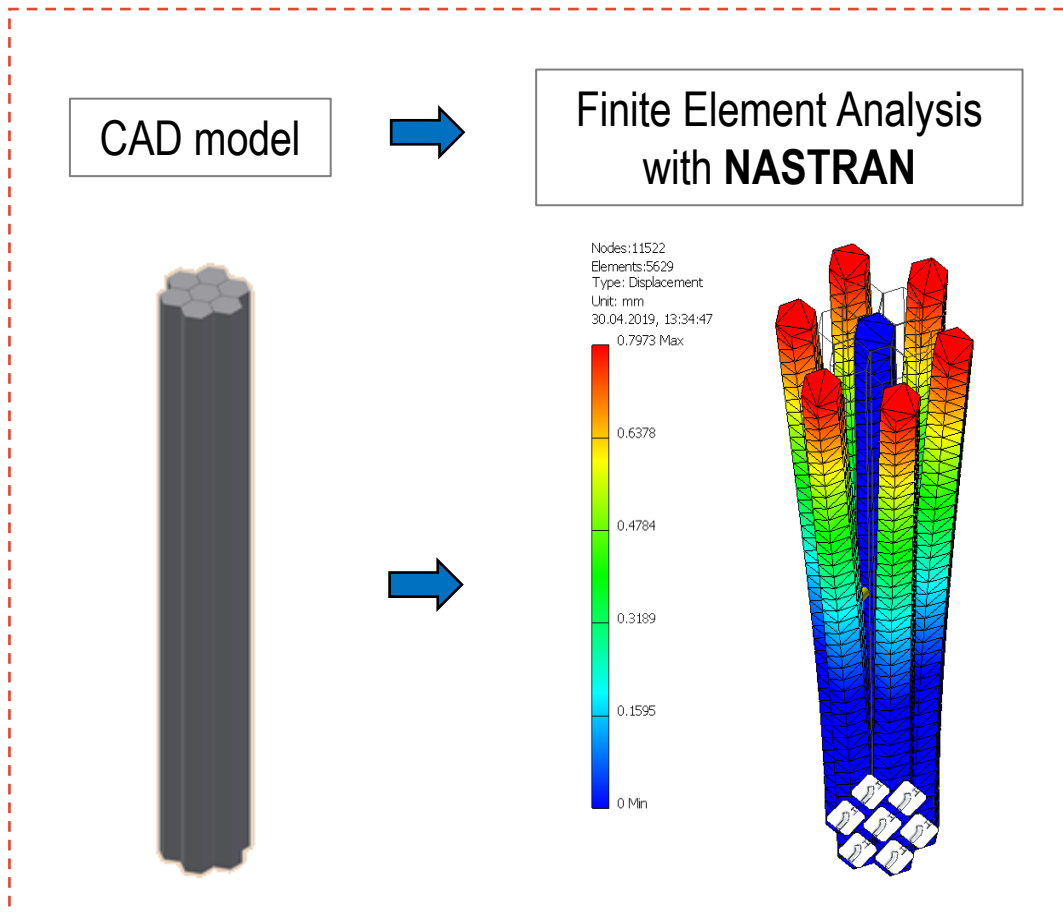
# Goals

- Methods development
  - To estimate core geometry distortions
  - To evaluate corresponding reactivity effects
- Dedicated WP in the ESFR-SMART project



# Modeling of mechanical core deformations (PSI)

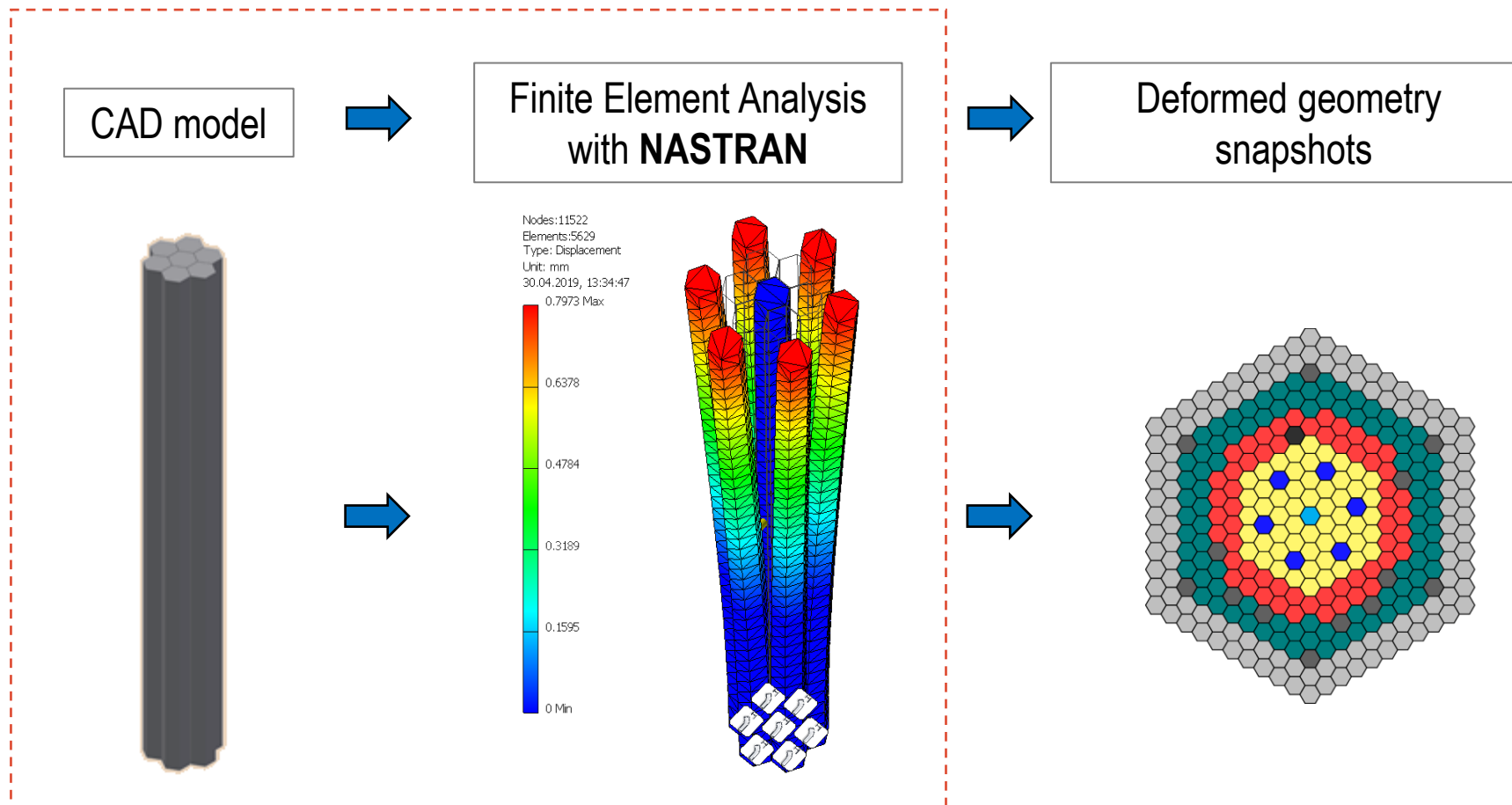
- Based on NASTRAN finite element solver





# Modeling of mechanical core deformations (PSI)

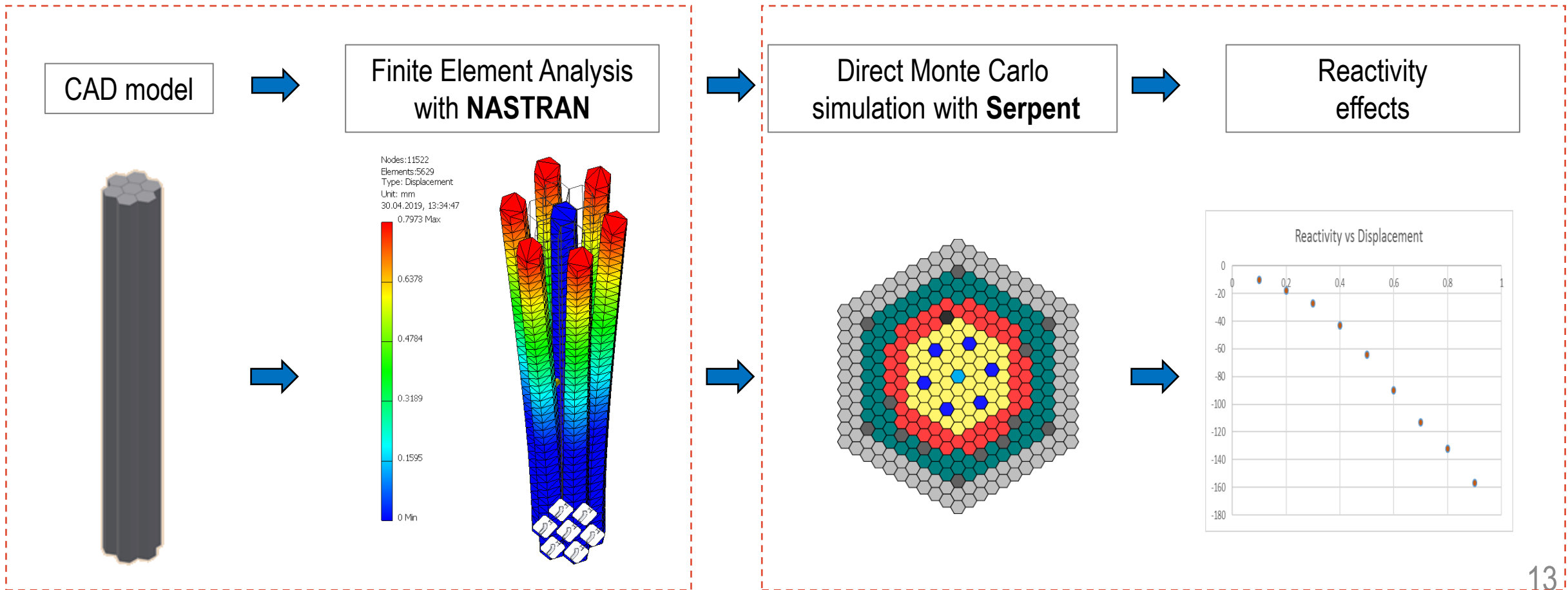
- Based on NASTRAN finite element solver





# Modeling of reactivity effects (PSI)

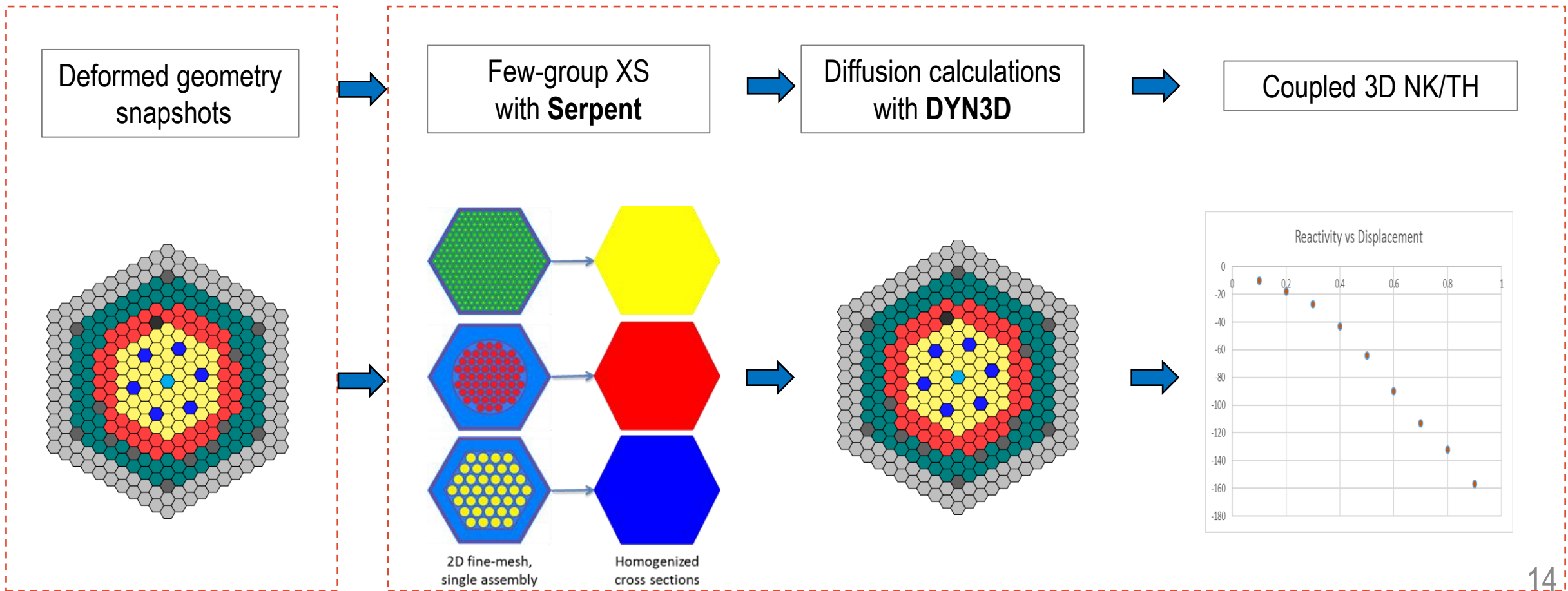
- Direct CAD-based Serpent simulations using NASTRAN geometry snapshots
- Reactivity coefficients for transient analysis with TH system code (coupled **0D** neutron kinetics/TH)





# Modeling of reactivity effects (HZDR)

- Based on Serpent and DYN3D (nodal diffusion)
- Transient analysis with DYN3D (coupled 3D neutron kinetics/TH)



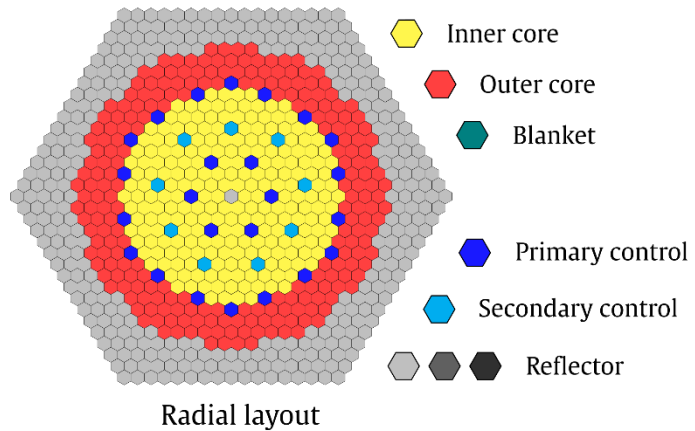
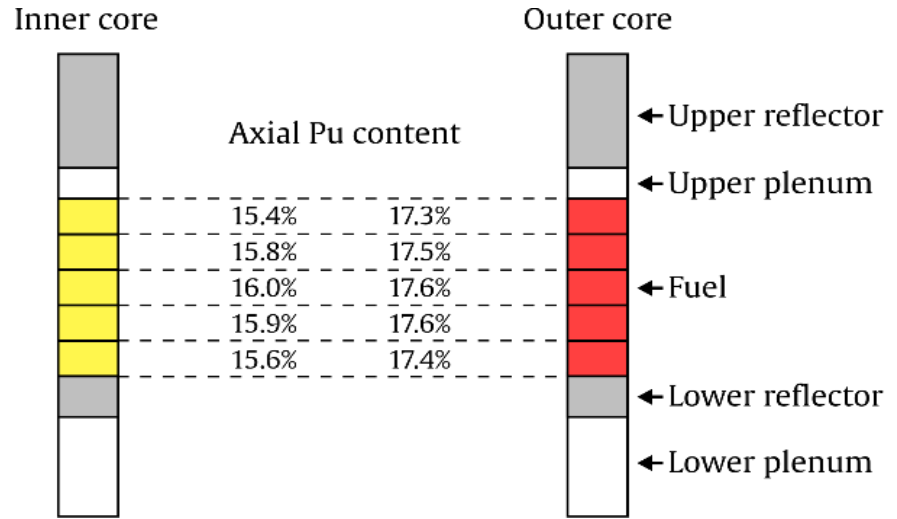


# Modeling of non-uniform radial expansions in DYN3D

- Using coordinate transformation method
- Allows to model non-uniform expansion using a fixed nodal mesh
- Applicable to nodal diffusion codes like DYN3D and PARCS
- No need to change the diffusion solver
- Only few-group XS should be adjusted



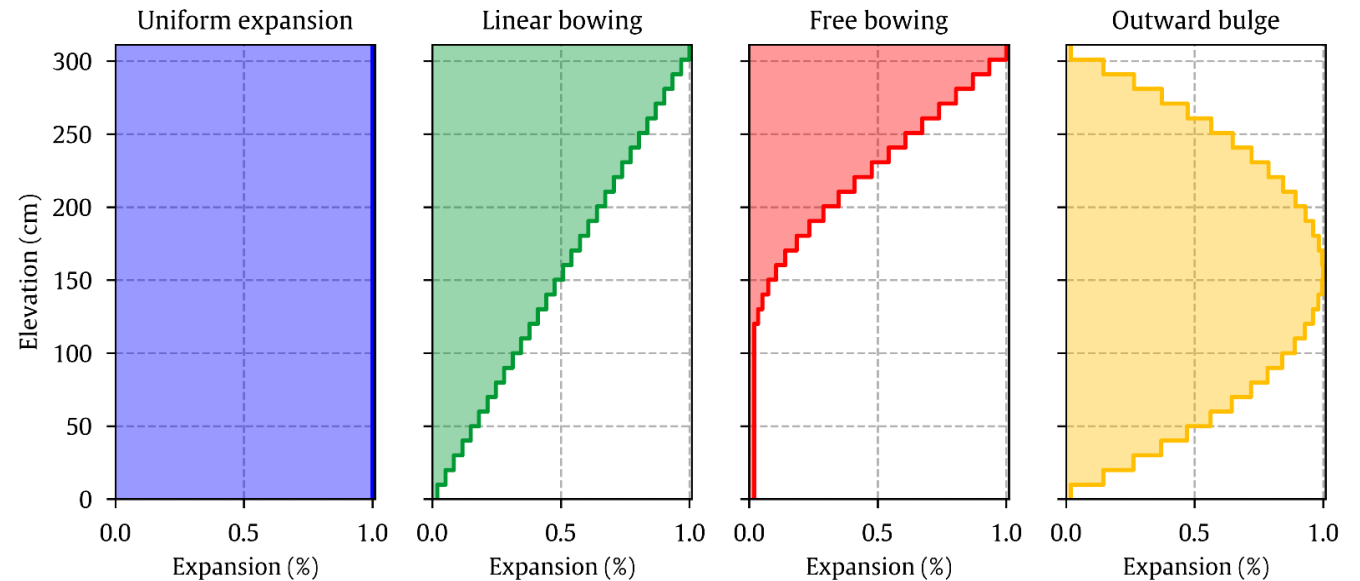
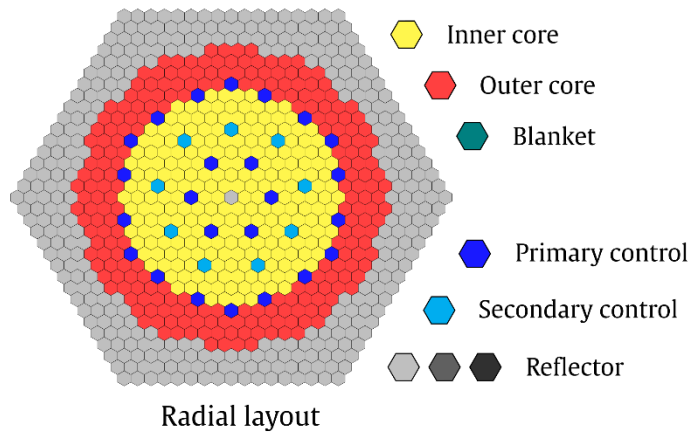
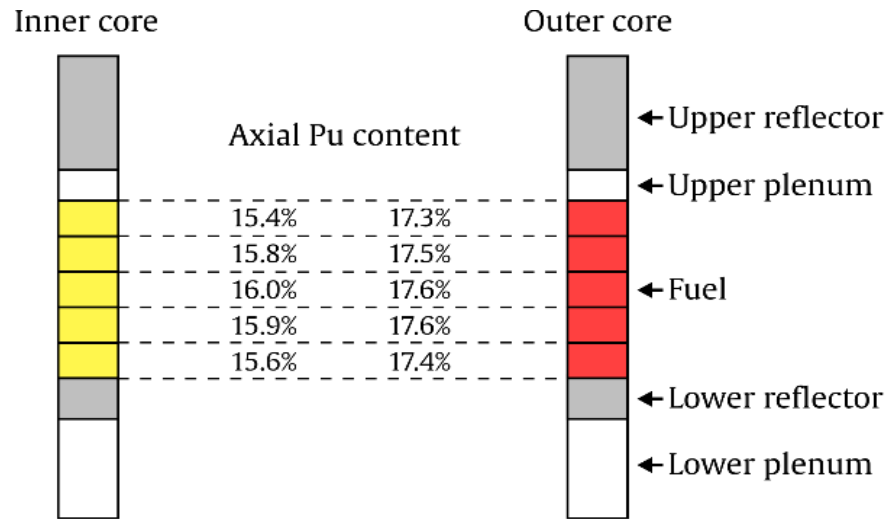
# Verification of the coordinate transformation method







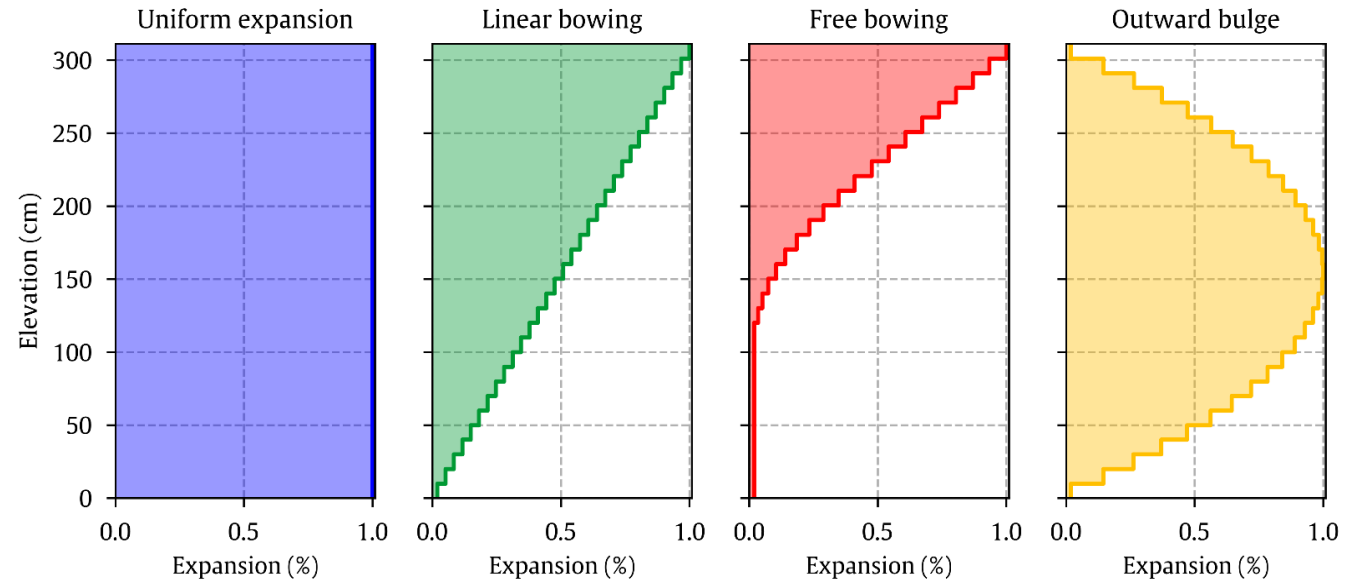
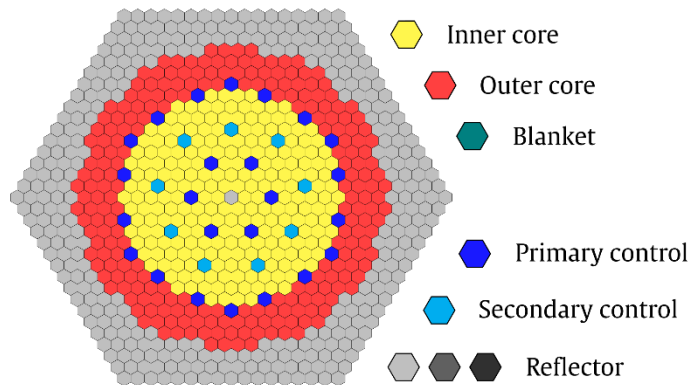
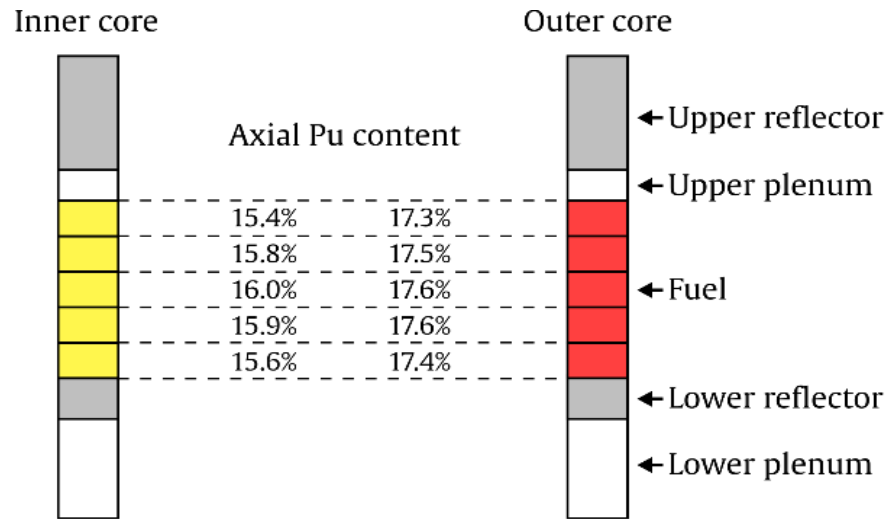
# Verification of the coordinate transformation method



- Verification of DYN3D vs. Serpent
- Serpent: realistic geometry deformations
- DYN3D: fixed mesh + coordinate transformation



# Verification of the coordinate transformation method



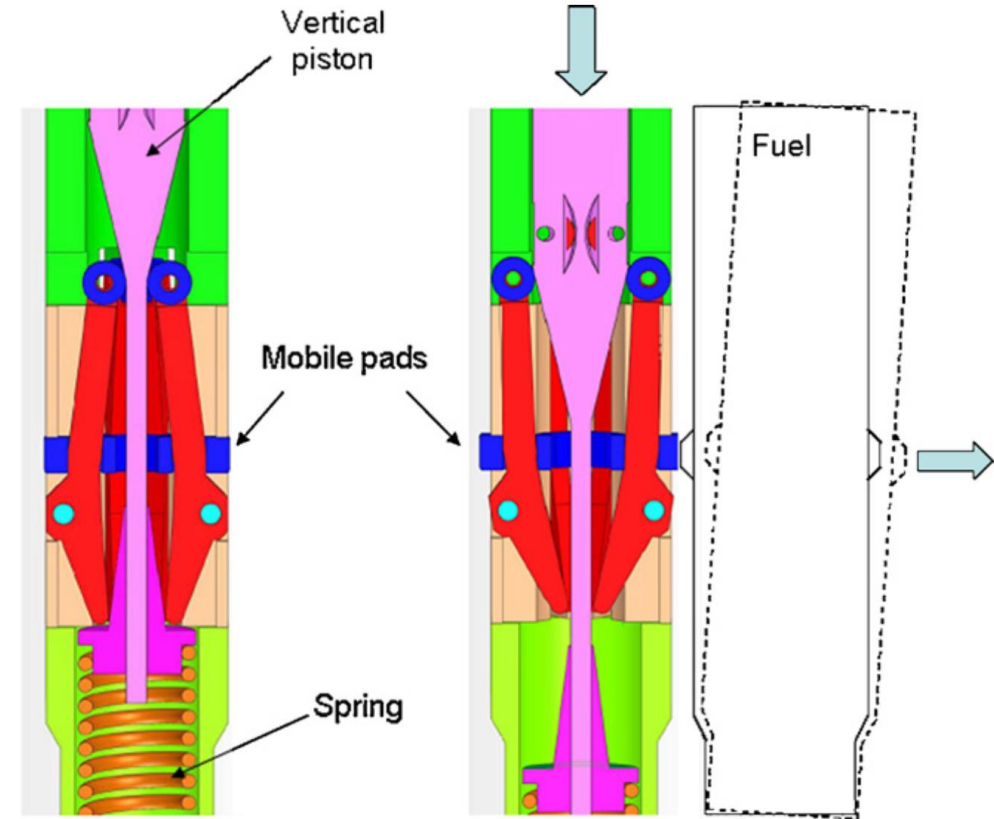
	Uniform	Linear bowing	Free bowing	Outward bulge
<b>Serpent, pcm</b>	-425	-230	-70	-405
<b>DYN3D, pcm</b>	-413	-223	-65	-398
<b><math>\Delta\rho</math>, pcm</b>	12	6	4	7

- Steady-state analysis of the Phenix “flowering” tests
- Transient analysis of the postulated Phenix core deformation case



# Validation using Phenix “flowering” tests

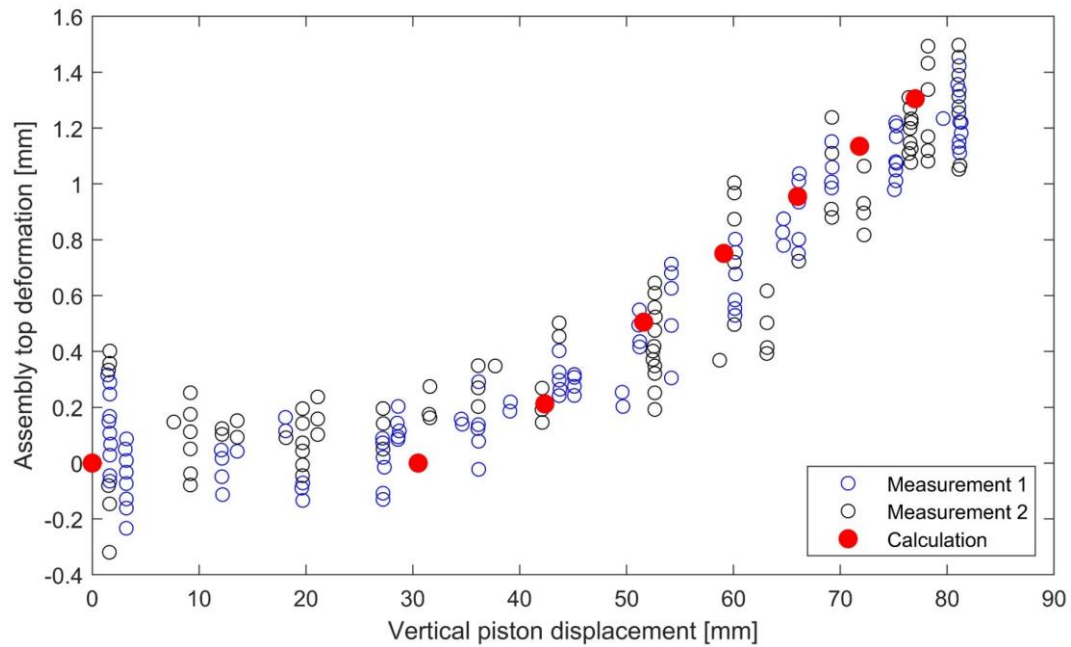
- Mechanical tests were conducted on the Phenix EOL core
- Identify potential reasons for “AURN”:
  - “Arrêt d’Urgence par Réactivité Negative”
  - 4 reactivity events at Phenix
- Step-wise deformations introduced by “flowering” device
- Reactivity effects were measured for every step
- The test was simulated with NASTRAN/Serpent





# Validation using Phenix “flowering” tests

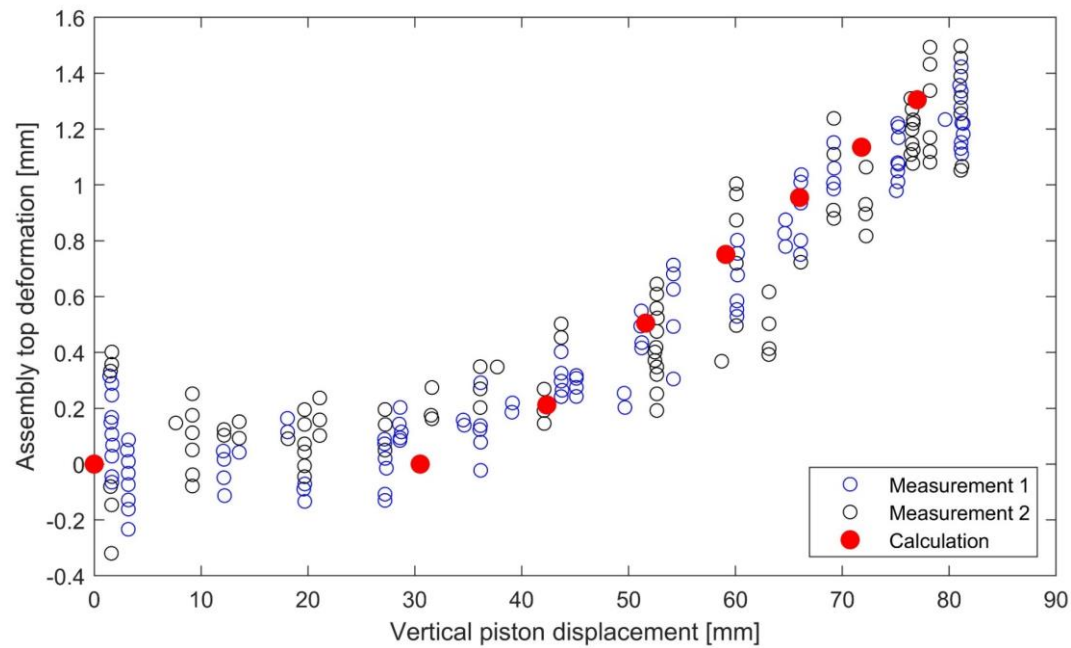
Displacement of the measured fuel assembly  
simulation vs. measurement



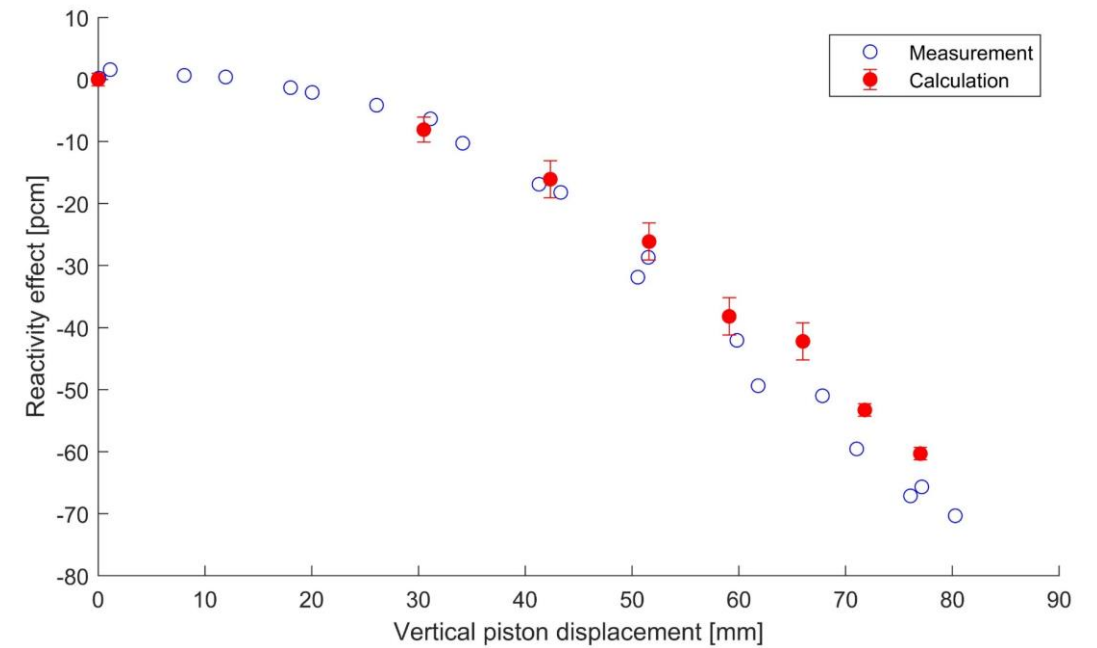


# Validation using Phenix “flowering” tests

## Displacement of the measured fuel assembly simulation vs. measurement



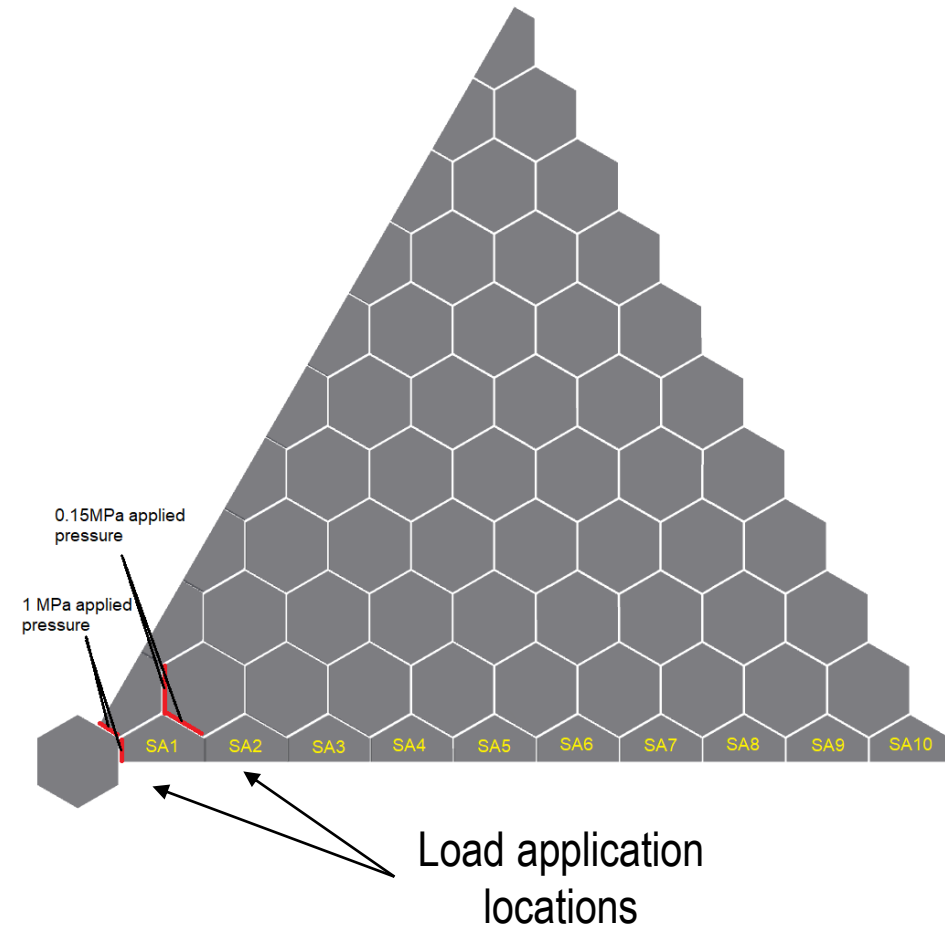
## Global reactivity effect of the “flowering” simulation vs. measurement





# Phenix transient analysis: Postulated scenario

- Core deformations due to pressure waves
  - 1 MPa pikes due to bubble collapse
  - Based on PSI ULOF simulation
- Loads applied to
  - SAs adjacent to the center
  - SA in the middle of second ring
  - Between fuel and SA tops
- Load duration = 30 msec
- Full simulation time = 210 msec
- Geometry snapshot at 15 time points





# Phenix transient analysis: Analysis stages

- Generate geometry snapshots
- Static Monte Carlo solution
  - CAD-based geometry models in Serpent
  - Set of static 3D calculations with geometry snapshots
- Static and dynamic DYN3D solution with 3D diffusion
  - Generate few-group XS using Serpent
  - **Set of static** 3D DYN3D calculations with geometry snapshots
  - **Single dynamic** 3D DYN3D calculation with dynamic geometry variation
- Dynamic TRACE solution with 0D NK
  - Incorporate new reactivity feedback in point kinetics
  - Transient calculations with system code TRACE

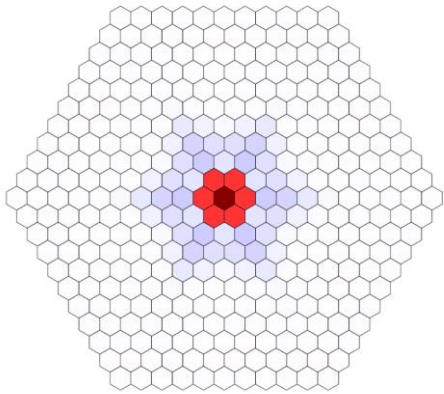




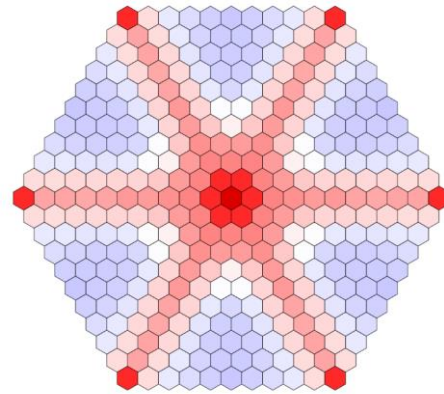
# Selected snapshots of Phenix core geometry

- Averaged change of inter-assembly gap (red – expansion, blue – compaction)

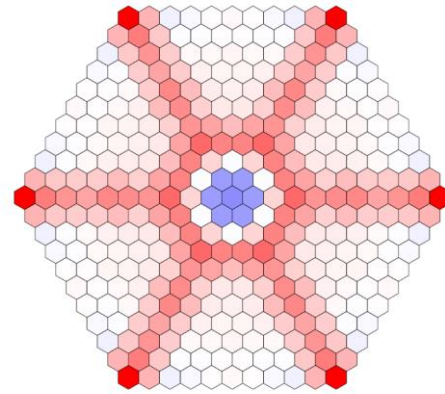
t = 15 ms



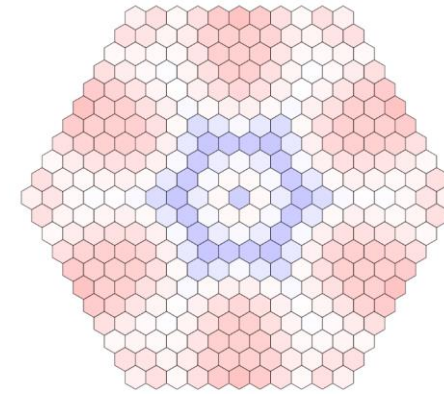
t = 45 ms



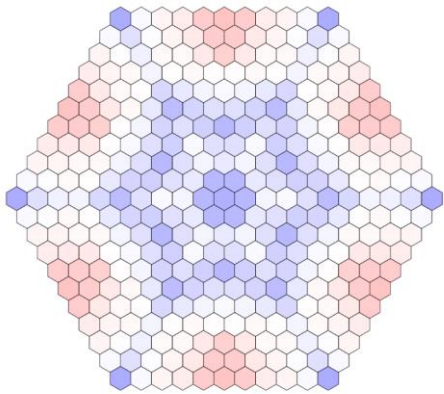
t = 75 ms



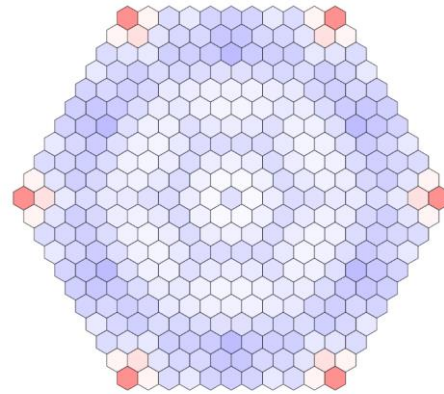
t = 105 ms



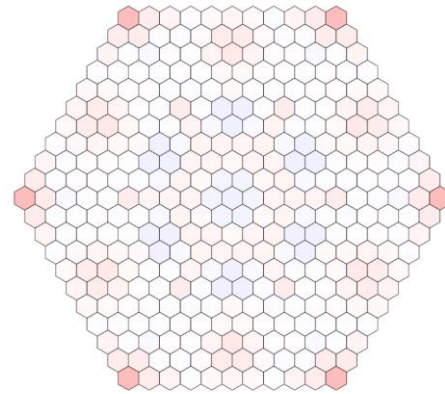
t = 120 ms



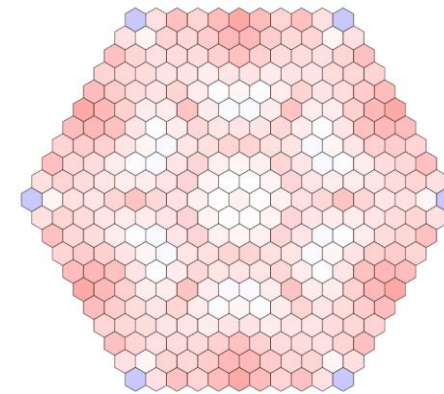
t = 150 ms



t = 180 ms



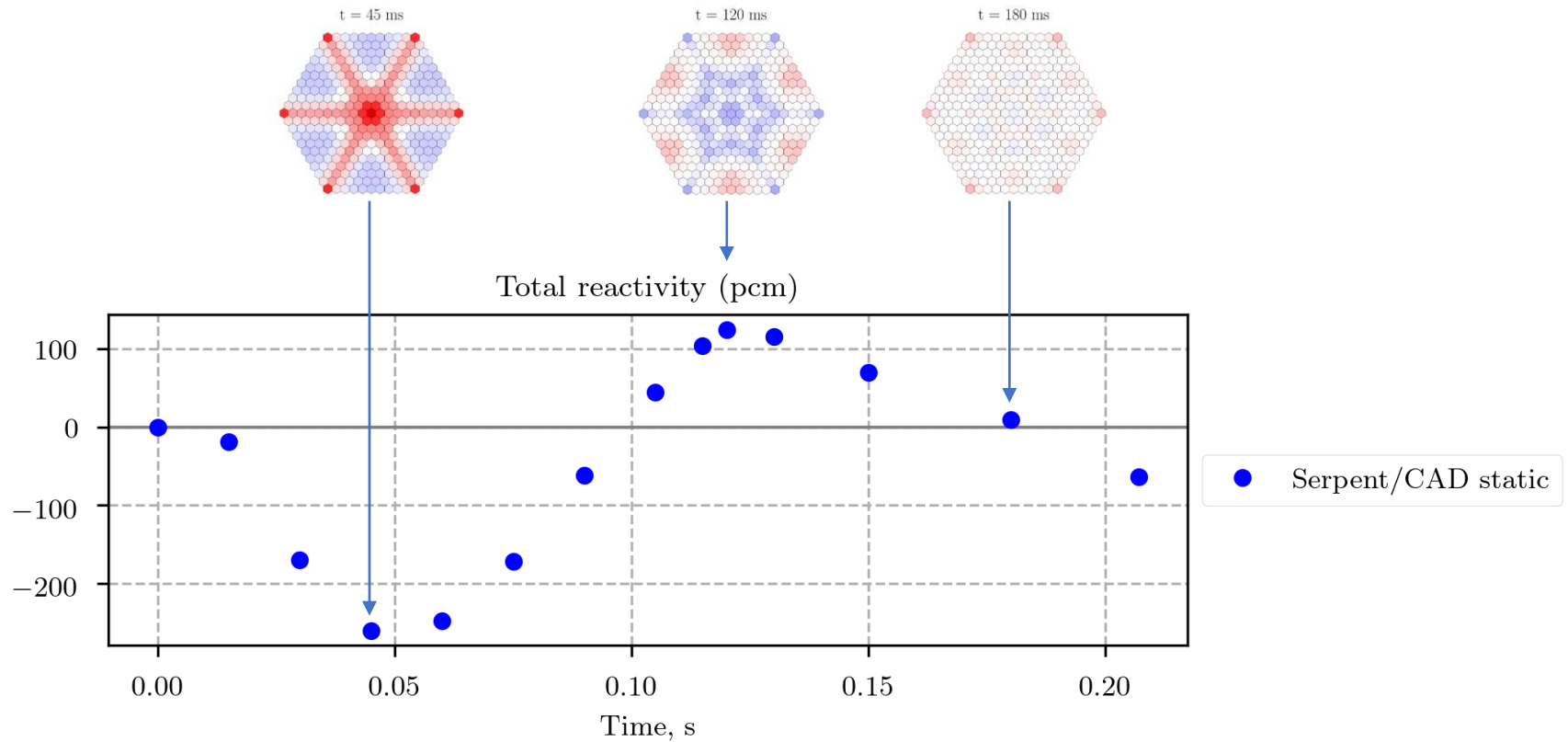
t = 207 ms





# Phenix core deformation: Static Serpent solution

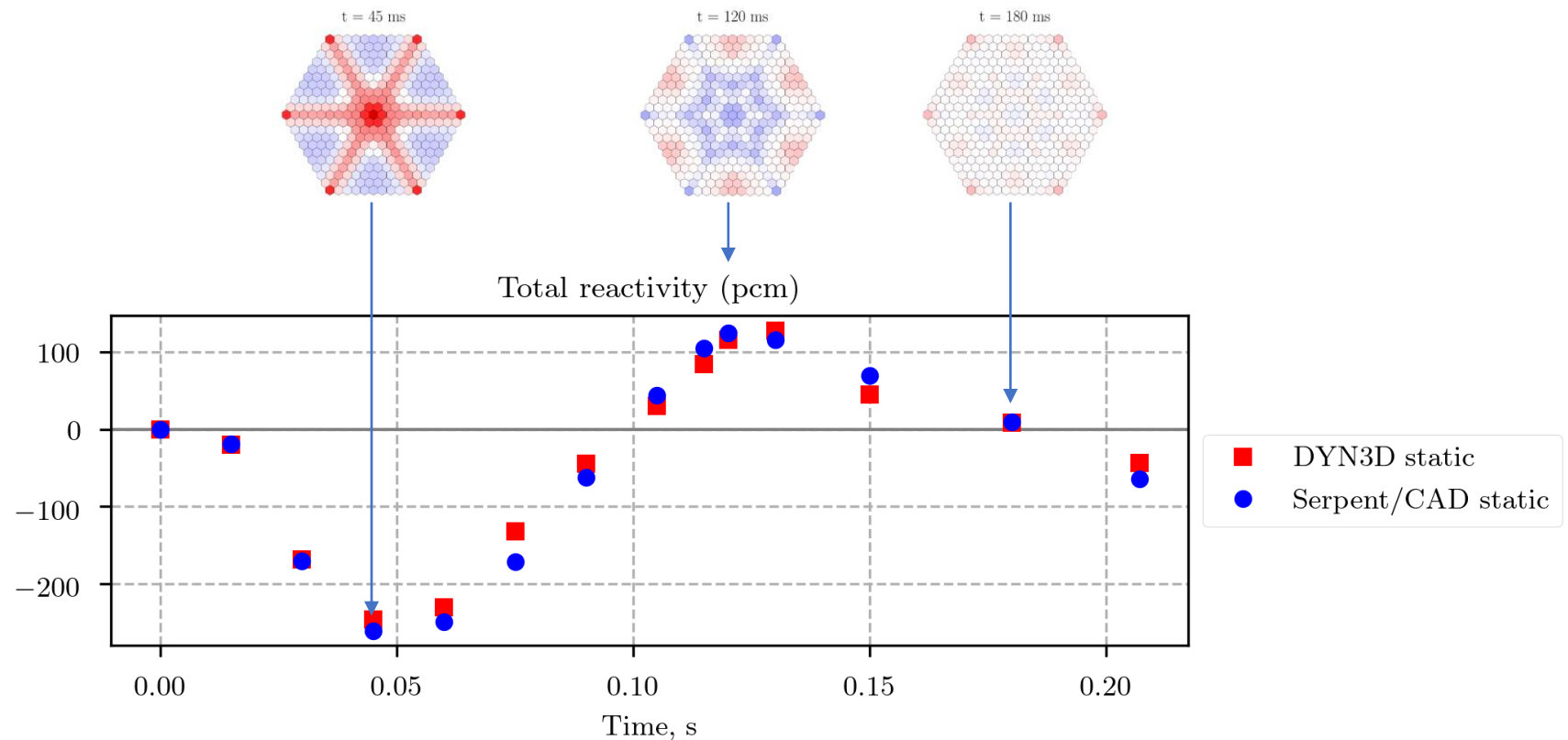
- Detailed CAD models for deformed geometries
- Static neutronic calculations for 14 geometry snapshots





# Phenix core deformation: Static DYN3D solution

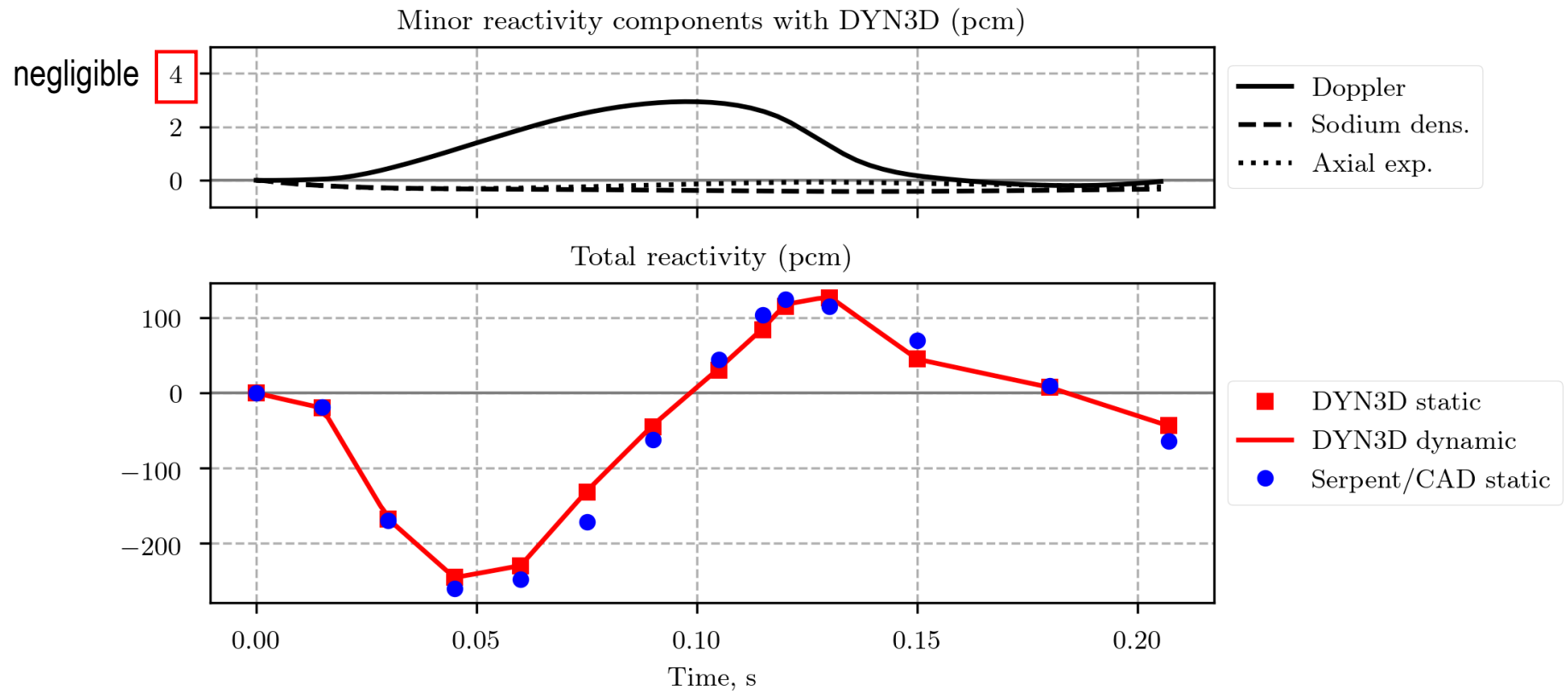
- Few group XS with Serpent
- Deformation of each node by Coordinate Transformation Method
- Numerical mesh remains regular and fixed





# Phenix core deformation: Dynamic DYN3D solution

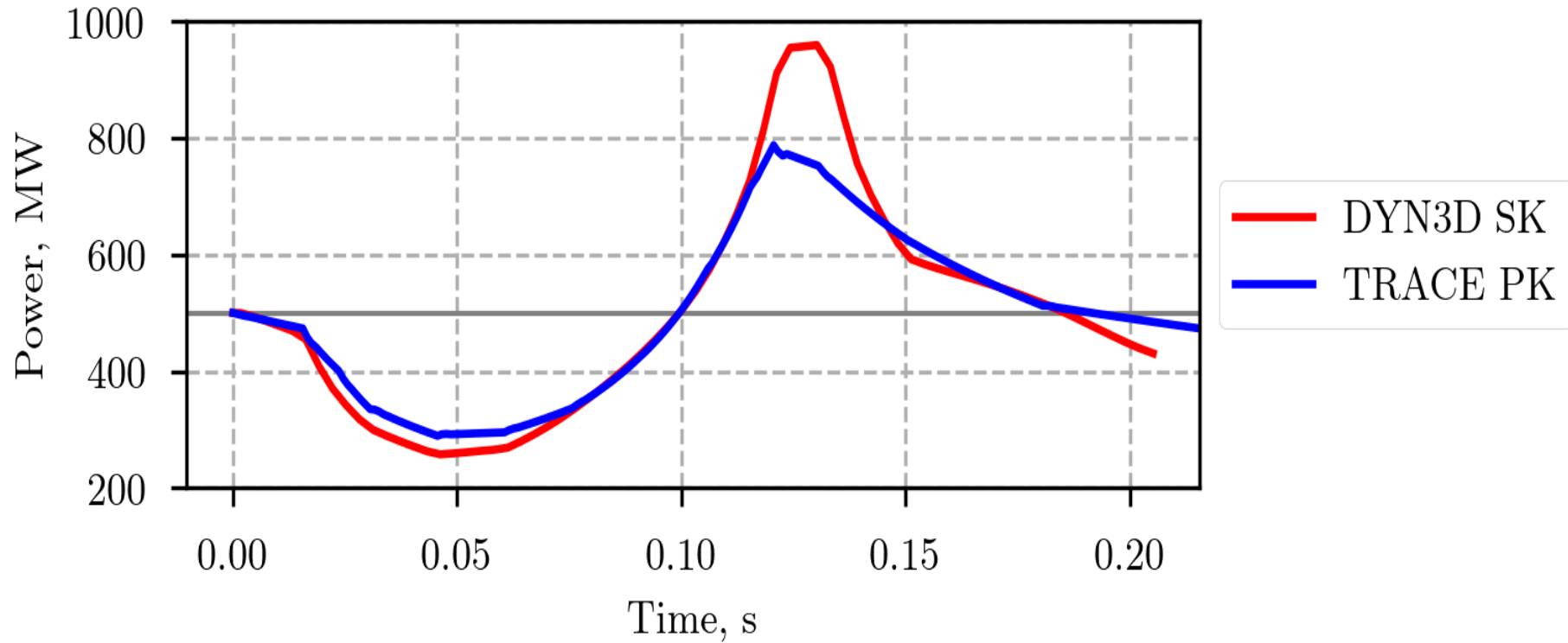
- 3D kinetics + TH feedback
- Reactivity fully driven by deformation
- Very good agreement between DYN3D and Serpent/CAD





# Phenix core deformation: 0D vs. 3D kinetics

- Good agreement between TRACE with point-kinetics vs. DYN3D with 3D kinetics



- Core deformation due to pressure waves
  - Modeling of core deformations is performed
  - Application to the Phenix and ESFR cores
  
- Reactivity effects due to core deformation
  - Established methodology for assessment of reactivity effects
  - Both 0D and 3D kinetics
  - Verification on the Phenix core



# Acknowledgment

- HZDR
  - Evgeny Nikitin
  - Alexander Ponomarev
  
- PSI
  - Janos Bodi
  - Konstantin Mikityuk

**Thank you!**

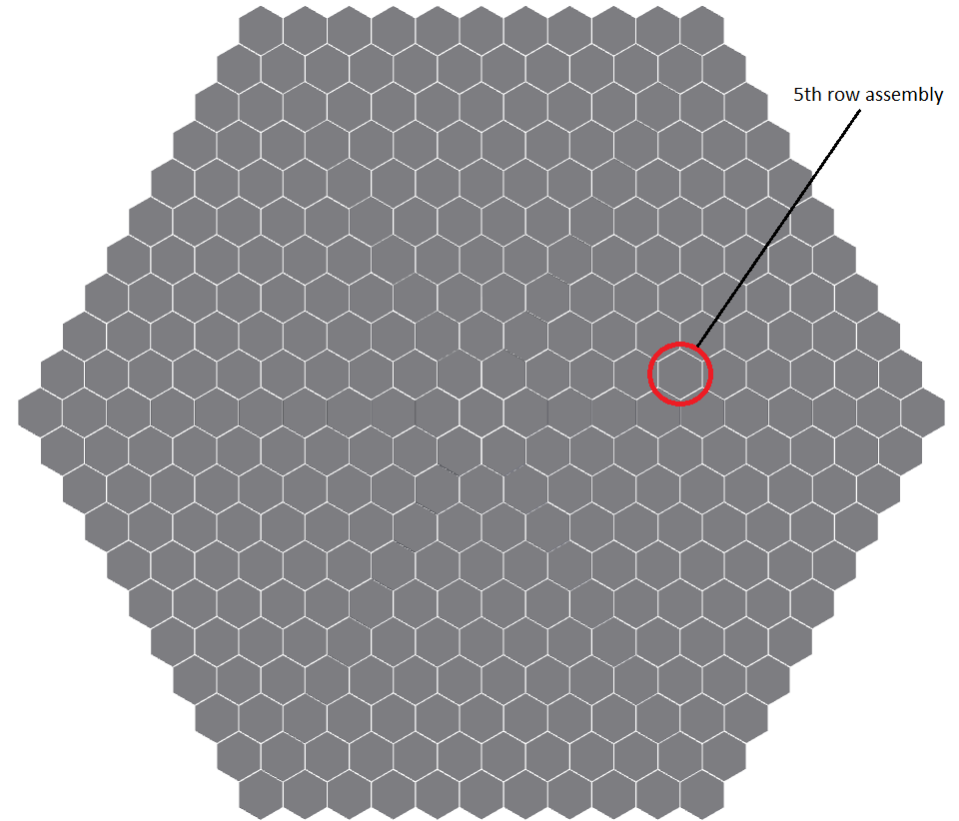
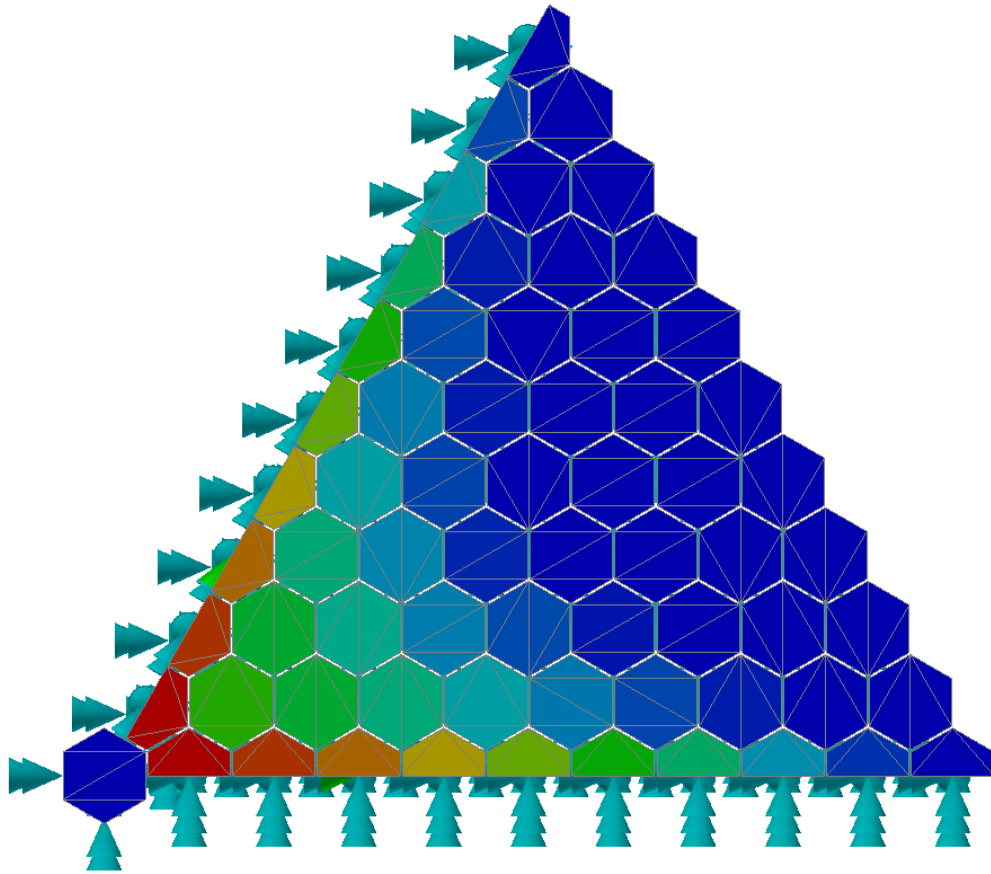
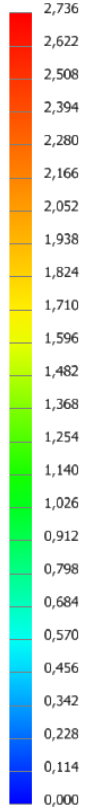






# Validation using Phenix “flowering” tests

Displacement [mm]









# Homogeneous Phenix core model

