

# High conversion Th-U<sup>233</sup> fuel assembly for current generation of PWRs

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September 15<sup>th</sup>, 2011



# OUTLINE

- Objectives
- Codes
- IAEA benchmark
- Fuel assembly design optimization
- Results
- Summary

# OBJECTIVES

- To improve utilization of natural resource in current PWRs
- Via the use of high conversion Th-U<sup>233</sup> fuel cycle
  - Heterogeneous seed-blanket fuel assembly design
  - In closed fuel cycle
- The assembly should be retrofittable into a PWR core
  - Typical 17x17 PWR lattice
  - Standard operating conditions
  - Without affecting the safety

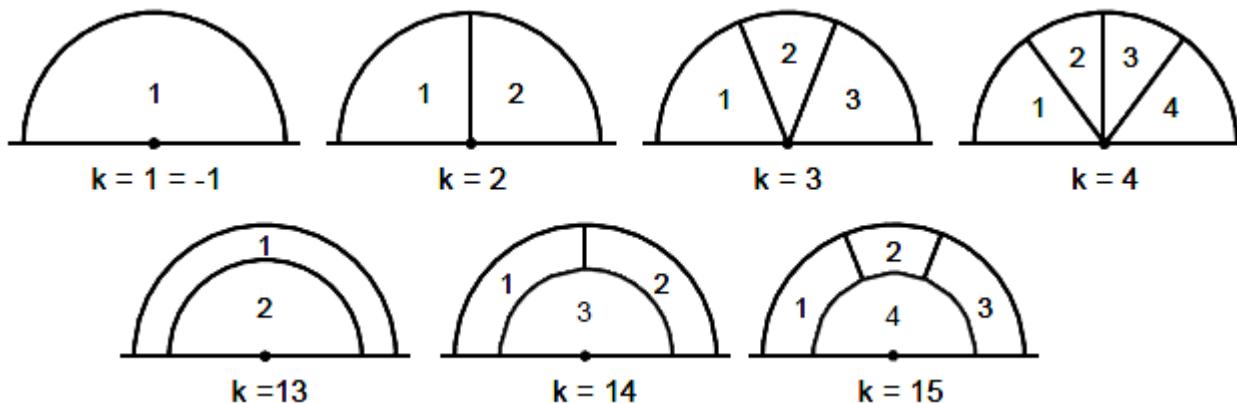
# CODES

- HELIOS
  - Lattice transport code
  - Collision probabilities with current coupling
  - Used as a production code in the study
- SERPENT
  - Used for:
    - Benchmarking purposes
    - Evaluation of spent fuel characteristics

# IAEA Th BENCHMARK

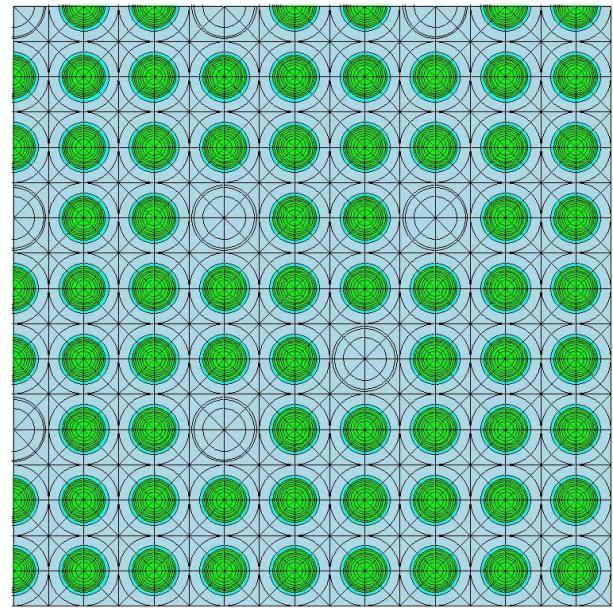
## Helios vs. Serpent

- To verify Helios capabilities for the Th based fuel analysis
- To find optimal setup options for Helios
  - Resonance categories, current coupling, discretization
  - No clear recommendation from developer



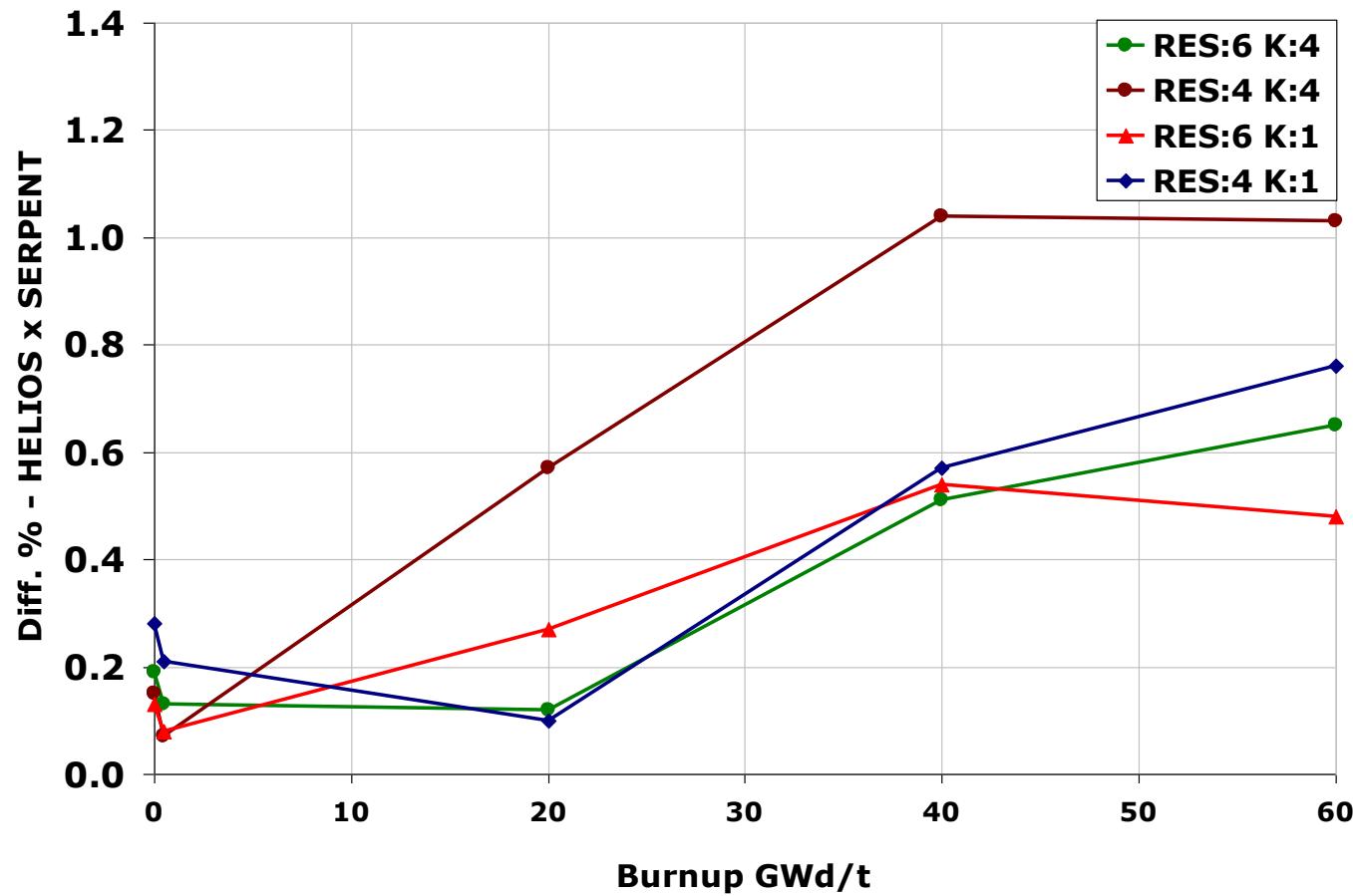
# IAEA BENCHMARK

- Fuel assembly parameters
- Th-Pu fuel
- 17x17 PWR fuel assembly lattice
- 25 water hole positions
- Power density of 37.7 MW/t

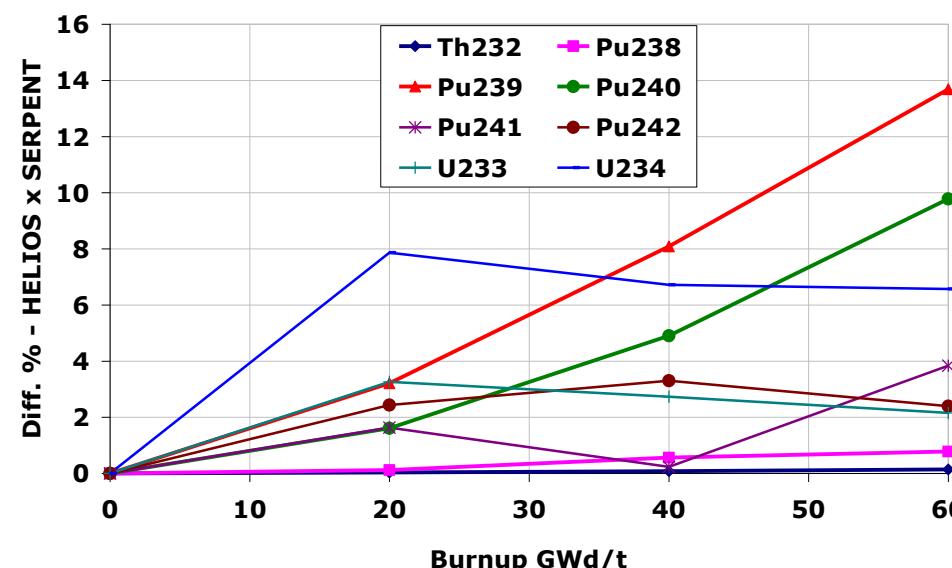


One quarter of fuel assembly

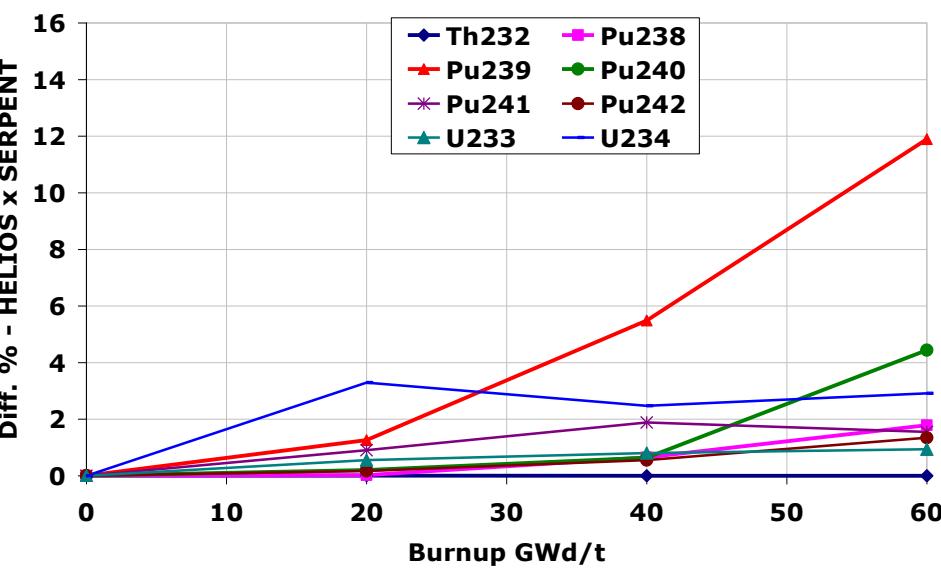
# IAEA benchmark results – Kinf Serpent vs. Helios



# IAEA benchmark results – Number densities Serpent vs. Helios



Res:6 K:4



Res:6 K:1

# IAEA benchmark results – Power map BOL Serpent vs. Helios

W									
1.10%	0.81%								
1.25%	0.85%	1.25%							
W	0.90%	0.87%	W						
0.39%	0.80%	0.85%	0.77%	0.04%					
0.61%	0.71%	0.59%	1.18%	1.18%	W				
W	1.42%	1.50%	W	1.62%	1.24%	0.37%			
0.51%	0.37%	0.51%	0.72%	0.40%	0.62%	1.12%	0.83%		
0.85%	1.56%	0.71%	0.74%	0.79%	0.87%	0.67%	0.80%	0.08%	

Max. error – 1.62 %

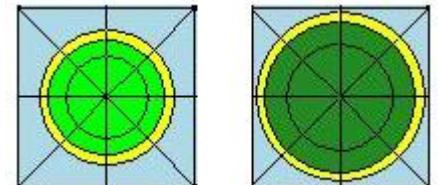
Average error – 0.75 %

Res:6 K:1

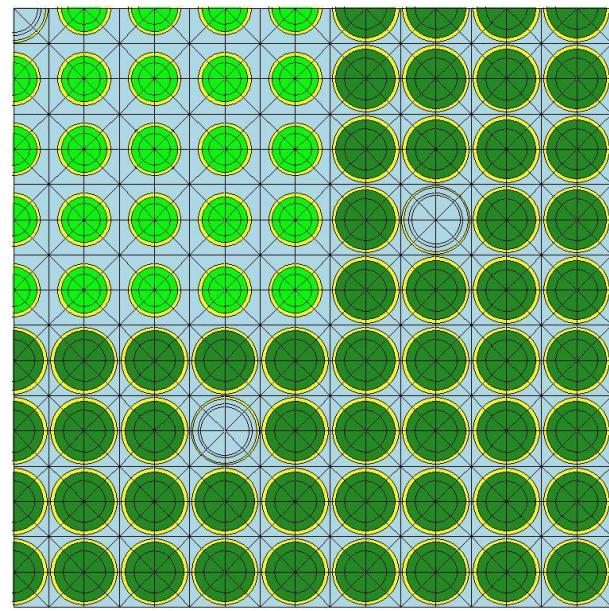
# FUEL ASSEMBLY DESIGN OPTIMIZATION

## Seed-Blanket fuel assembly design

- Th-U<sup>233</sup> Fuel
- Typical 17x17 PWR lattice
- 80 seed and 200 blanket pins
- 9 guide tubes
- Seed pin radius – 0.4095 cm
- Blanket pin radius – 0.5300 cm (Enlarged)
- Power density 70 W/cm<sup>3</sup>
  - High peaking in seed



Seed      Blanket



One quarter of 17x17 SB  
fuel assembly

# FUEL ASSEMBLY DESIGN OPTIMIZATION

## Methodology

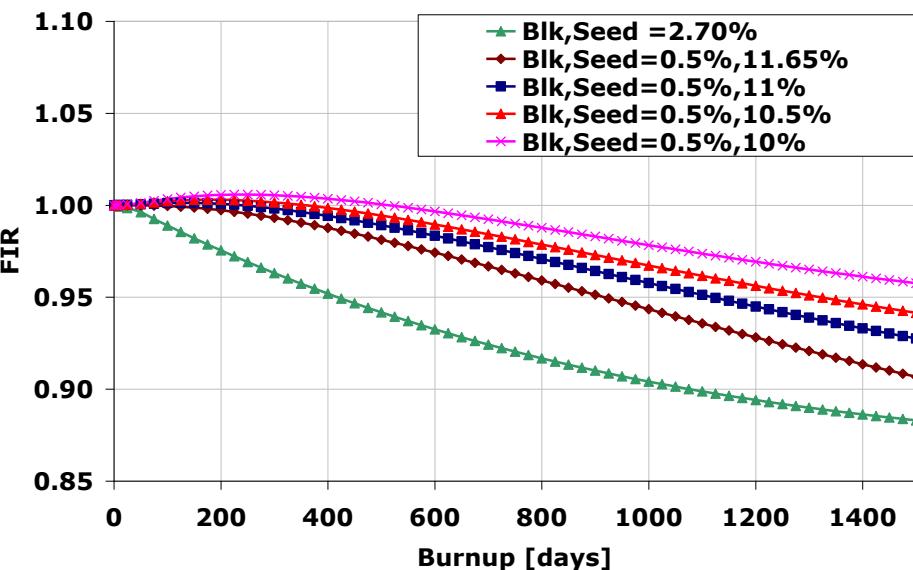
- 2D fuel assembly level
- Non Linear Reactivity Model
  - For estimation of  $k_{\text{eff}}$  and fuel cycle length
- To calculate
  - Fissile inventory ratio (FIR)
  - Fuel cycle length
  - $K_{\text{eff}}$  core
  - Local pin-by-pin power distribution
  - Activity of discharged fuel
- Constraints
  - 3 batches, 18 month fuel cycle
  - $K_{\text{eff}} > 1$  during the fuel cycle

# FUEL ASSEMBLY DESIGN OPTIMIZATION

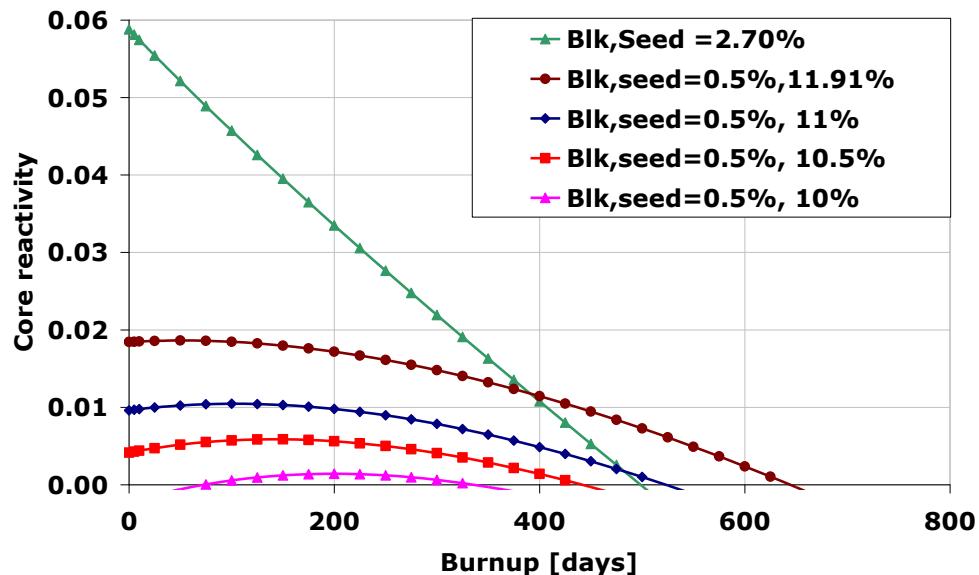
## Strategy

- Start with the equal seed and blanket enrichment
  - Adjust the enrichment to achieve the desired fuel cycle length
- Decrease enrichment in blanket while keeping the total U<sup>233</sup> amount
- Decrease enrichment in seed while keeping the enrichment in blanket

# RESULTS obtained by Helios



Fissile inventory ratio



Core reactivity

For optimized fuel assembly:

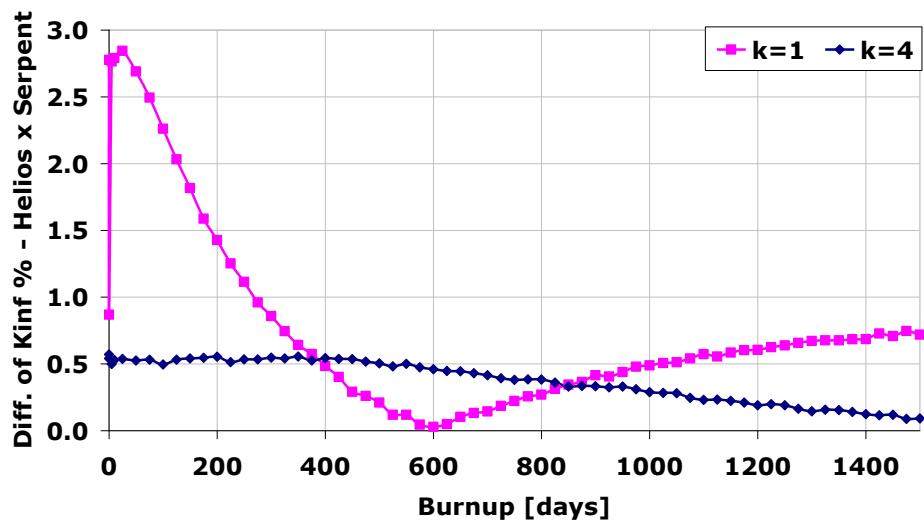
- FIR = 0.95
- Fuel cycle length = 440 EFPD

# RESULTS obtained by Helios

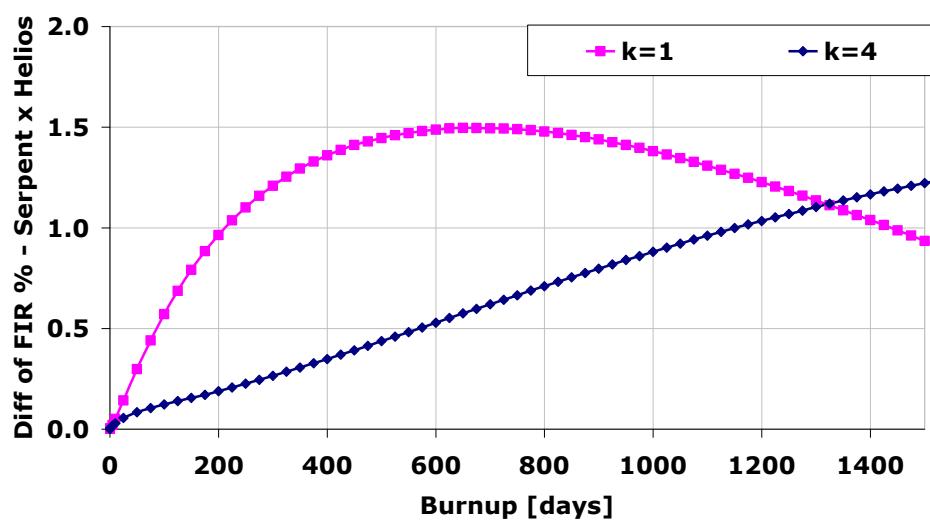
## Power map

W									
1.43	2.77								
1.35	2.69	2.69							
1.37	2.74	2.77	2.85						
1.49	2.99	3.04	3.13	3.32					
0.18	0.37	0.38	0.40	0.40	0.41				
0.20	0.40	0.41	W	0.42	0.41	0.41			
0.20	0.41	0.42	0.43	0.42	0.41	0.41	0.41		
0.20	0.41	0.41	0.42	0.42	0.41	0.41	0.41	0.41	

# RESULTS confirmation with SERPENT



Difference of Kinf



Difference of FIR

# RESULTS confirmation with SERPENT

## Differences in power map

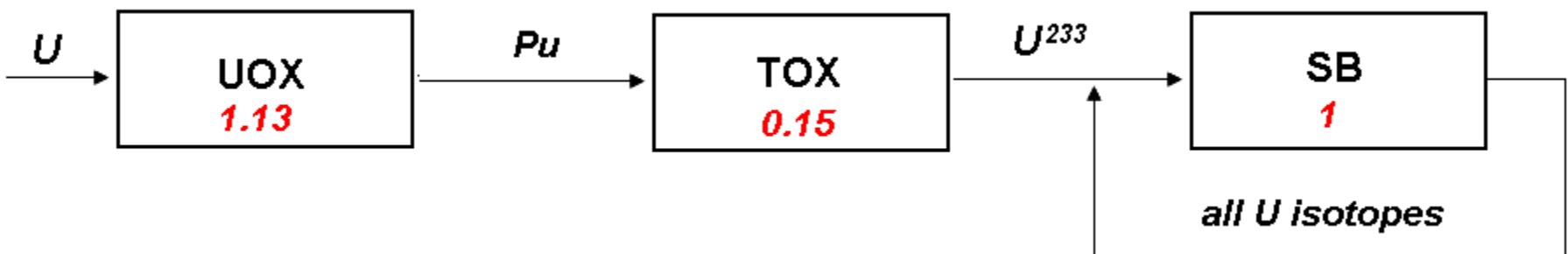
W										
0.61%	0.60%									
0.63%	0.42%	0.63%								
0.69%	0.70%	0.52%	0.77%							
0.40%	0.69%	0.45%	0.73%	0.05%						
0.36%	0.36%	0.54%	0.19%	0.77%	0.80%					
0.07%	0.08%	0.53%	W	0.53%	0.60%	0.47%				
0.14%	0.57%	0.88%	0.27%	0.78%	0.62%	0.74%	0.45%			
0.38%	0.35%	0.12%	0.07%	0.56%	0.83%	0.76%	0.50%	0.50%		

Max. error – 0.88 %

Average error – 0.52 %

# PRODUCTION OF U<sup>233</sup>

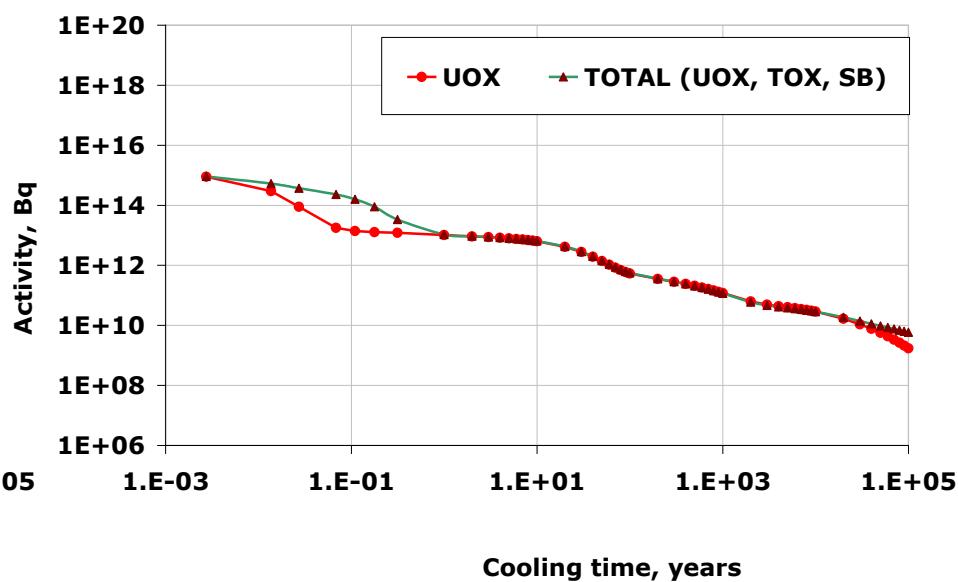
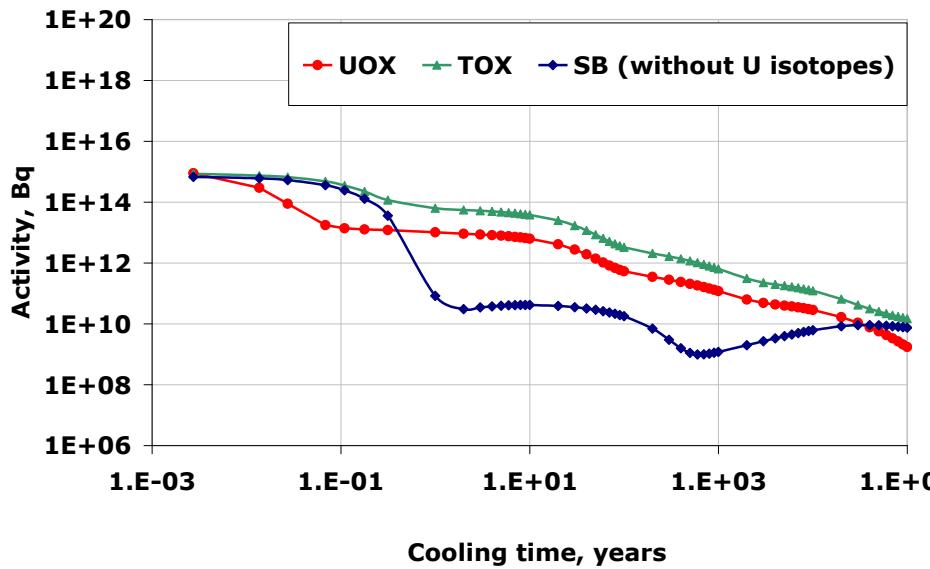
- Creation of U<sup>233</sup> is necessary
  - Initial
  - Makeup (FIR<1)
- How to create U<sup>233</sup>:
  - UO<sub>2</sub>-ThO<sub>2</sub>
  - PuO<sub>2</sub>-ThO<sub>2</sub> (TOX)
- How many UOX and TOX cores are needed at equilibrium:



## ENERGY BALANCE

$$\text{UOX} \quad 1 \quad + \quad \text{TOX} \quad 0.13 \quad + \quad \text{SB} \quad 0.88 * 0.7 = 1.75$$

# ACTINIDES ACTIVITY IN DISCHARGED FUEL



- Calculated by Serpent
- Depletion till 1350 EFPD
- Decay till  $10^5$  years

# CONCLUSION

- Helios verifications
  - Results in good agreement with Serpent
- For optimized Th-U233 assembly:
  - FIR of about 0.95 can be achieved
  - Generation of  $U^{233}$  in TOX core was considered
  - 75% increase in NU utilization
  - No decrease in the discharged fuel activity
- Future work:
  - Detailed T-H analysis
  - Demonstration of sufficient shutdown margins
  - Confirmation of 2D results via full core calculations

# Thank you for your attention!